# Constrained multispectrum analysis of CO<sub>2</sub>–Ar broadening at 6227 and 6348 cm<sup>-1 1</sup>

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Abstract: We report the first extensive experimental measurements of Ar-broadened half-width and pressure-induced shift coefficients, speed dependence parameters, and line mixing coefficients for the  $30013 \leftarrow 00001$  and  $30012 \leftarrow 00001$  bands of  ${}^{16}O^{12}C^{16}O$  centered near 6227 and 6348 cm<sup>-1</sup>, respectively. These parameters were determined from 15 self-broadened and six Ar-broadened CO<sub>2</sub> spectra recorded at room temperature with long absorption path lengths (25 to 121 m) using the McMath–Pierce Fourier transform spectrometer (FTS) at the National Solar Observatory. All 21 spectra were fit simultaneously using a multispectrum nonlinear least-squares technique. The line positions and line intensities were constrained to quantum mechanical expressions to obtain maximum accuracies in the retrieved parameters. Speed-dependent line shapes with line mixing (via the relaxation matrix formalism) were required to remove systematic errors in the fit residuals using only the Voigt profile. Remaining fit residuals were minimized by adjusting the half-width and pressure-induced shift coefficients of the overlapping  $31113 \leftarrow 01101$  and  $31112 \leftarrow 01101$  hot bands. We compare the Ar-broadening parameters with those recently determined for self- and air-broadening in the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands and also with other Ar-broadening values from the literature, as appropriate.

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**Résumé :** Nous présentons les premiers résultats expérimentaux complets de l'étalement de la demi- largeur de ligne dû à la présence d'argon et des coefficients de déplacement de ligne induits par la pression, les paramètres de dépendance en pression et les coefficients de mélange de ligne pour les bandes de  $30013 \leftarrow 00001$  et  $30012 \leftarrow 00001$  du <sup>16</sup>O <sup>12</sup>C<sup>16</sup>O centrés près de 6227 et 6348 cm<sup>-1</sup> respectivement. Nous avons déterminé ces paramètres à partir de 15 spectres de CO<sub>2</sub> auto-élargis et six spectres avec élargissement causé par la présence d'argon, enregistrés à température de la pèce et avec les longs chemins d'absorption (25 à 121 m) du spectromètre McMath-Pierce à transformée de Fourier (FTS) du National Solar Obversatory. Nous avons simultanément ajusté mathématiquement l'ensemble des 21 spectres à l'aide d'une méthode de moindres carrés multispectrale et non linéaire. Les positions et intensités de ligne ont été ajustées aux expressions de la mécanique quantiques pour garantir un maximum de précision des paramètres extraits de l'analyse. Nous avons dû inclure une dépendance en vitesse de la forme des lignes et un mélange de lignes (via le mécanisme de la matrice de relaxation) afin d'éliminer les erreurs systématique dans les ajustements résiduels utilisant des profils de Voigt purs. Les autresajustements résiduels ont été minimisés en utilisant la demi-largeur et les coefficients de déplacement de ligne induit par la pression des bandes chaudes se recouvrant  $31113 \leftarrow 01101$  et  $31112 \leftarrow 01101$ . Nous comparons nos résultats d'élargissement causés par l'argon avec ceux obtenus récemment d'élargissement par l'air dans les bandes  $30012 \leftarrow 00001$  et  $30013 \leftarrow 00001$ , ainsi qu'avec d'autres résultats dans la littérature concernant un élargissement par l'argon.

[Traduit par la Rédaction]

# 1. Introduction

Accurate line positions, absolute line intensities, self- and air-broadened half-width and pressure-induced shift coefficients for transitions of the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands of  ${}^{16}O^{12}C^{16}O$  have recently been reported [1–7]. Line mixing and speed dependence for the majority of the

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transitions in these bands were also determined [4, 5] to minimize most of the systematic residuals using a constrained multispectrum fitting technique [8]. These data provide the CO<sub>2</sub> spectroscopic reference standards necessary to retrieve mixing ratios with uncertainties approaching 0.3% from observations to be made by the Orbiting Carbon Observatory (OCO) [9] and the Total Column Carbon Observing Network (TCCON) [10]. The primary goal of the present study is to provide accurate CO<sub>2</sub> spectroscopic reference standards for Ar-broadening parameters in the same spectral regions (6280 to 6395 cm<sup>-1</sup> and 6120 to 6280 cm<sup>-1</sup>) studied in [4, 5].

Despite the extensive investigations of CO<sub>2</sub>–Ar infrared spectra [11–32], there have been only three previous studies of Ar-broadened CO<sub>2</sub> spectra in the region 6100–6400 cm<sup>-1</sup>. Valero and Suarez [11] determined the pressure-broadened half-width coefficients for the 30012 $\leftarrow$ 00001 band from 0.075 cm<sup>-1</sup> resolution Fourier transform spectrometer data, using the equivalent width method to analyze each spectral line for each sample condition. They measured the Ar-

Pure CO <sub>2</sub>			CO <sub>2</sub> in argo	on		
Temp (K)	Pressure <sup>a</sup> (torr)	Path length (m)	Temp (K)	Pressure (torr)	CO <sub>2</sub> volume mixing ratio	Path length (m)
293.99	896.84	49.00	294.41	902.17	0.0617	121.18
293.68	556.56	49.00	293.84	621.41	0.0892	121.18
293.49	252.42	49.00	293.70	248.87	0.0625	121.18
293.09	52.14	49.00	293.47	100.14	0.0619	121.18
293.89	450.93	24.94	294.37	550.50	0.0500	24.94
293.88	101.95	24.94	294.18	50.06	0.0505	24.94
293.94	26.10	24.94				
294.05	11.04	24.94				
293.37	252.01	2.46				
294.37	94.65	2.46				
293.58	75.27	2.46				
294.09	50.70	2.46				
292.79	30.31	2.46				
293.57	25.61	2.46				
293.38	9.973	2.46				

Table 1. Summary of experimental conditions of the CO<sub>2</sub> and CO<sub>2</sub>-Ar spectra.

<sup>a</sup>Pure (natural) CO<sub>2</sub> samples (volume mixing ratio = 1 with 0.9842  $^{16}O^{12}C^{16}O$ ). 1 atm = 101.3 kPa = 760 torr.

broadened half-width coefficients at 197, 233, and 294 K, although they did not determine the temperature dependence exponents of the half-width coefficients. Suarez and Valero [12] did a similar study for the 30013←00001 band. Nakamichi et al. [30] determined Ar-broadened half-width coefficients for the R0, P8, P16, P26, and P38 of the 30013← 00001 band from spectra recorded with a diode laser based continuous wave (cw) cavity ring-down spectrometer. They employed a Voigt function in their analysis. Recently, room temperature air- and Ar-broadened half-width coefficients were reported by Li et al. [32] for 11 R-branch transitions (R0-R20) in the  $30012 \leftarrow 00001$  band. Their data were obtained with a photo acoustic spectrometer in conjunction with a high-resolution tunable diode laser, and analysis was performed employing a standard Voigt line shape on individual spectral lines.

Line mixing effects in CO<sub>2</sub>–Ar spectra have been reported by several investigators using energy corrected sudden (ECS) calculations [e.g., 18, 19, 21, 23, 24]. In particular, Ozanne et al. [21] reported experimental and theoretical results on CO<sub>2</sub>–Ar spectra in the  $v_3$  and  $3v_3$  bands. At pressures of 100–1000 bars (1 bar = 100 kPa) they observed interbranch (R $\leftrightarrow$ P) line mixing on the spectral shapes. Filippov et al. [18] analyzed the absorption coefficients in the  $3v_3$  band of CO<sub>2</sub> at pressures up to 146 bar using two theoretical line-mixing calculations within the impact approximation. Rachet et al. [16] studied line mixing effects in the  $20001\leftarrow01101$  and  $12201\leftarrow01101$  Q branches located near 2130 and 2093 cm<sup>-1</sup> of the spectra of CO<sub>2</sub>, in mixtures with  $N_2$ , O<sub>2</sub> and Ar.

To our knowledge the only studies that have been reported on the temperature dependence exponents for  $CO_2$ -Ar collision broadening coefficients are by Brownsword et al. [15] and Wooldridge et al. [20]. Wooldridge et al. [20] used a cw lead-salt diode laser and studied the R48-R52 transitions of the  $v_3$  band of  $CO_2$  in the temperature range of  $\sim 297 - 2293$  K. They compared their  $CO_2$ -Ar half-width coefficients with prior experimental investigations

and also reported a value of 0.61 as the temperature dependence exponent, which is quite different from the value of  $0.88 \pm 0.18$  published by Brownsword et al. [15].

In this paper, accurate measurements of Ar-broadened half-width and Ar-induced pressure shift coefficients are reported for the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands of  ${}^{16}O^{12}C^{16}O$  for transitions up to J'' = 62. In addition to the broadening parameters, line mixing coefficients via the relaxation matrix formalism [33] and speed dependence were required to remove most of the systematic residuals from the least-squares fits. A critical difference between the present study and the works of Valero and Suarez and Suarez and Valero [11, 12] is that the present study employed a multispectrum analysis that fit simultaneously all experimental spectra over the entire spectral interval for each band (6120 to 6280 cm<sup>-1</sup> for the 30013 $\leftarrow$ 00001 band and 6280 to 6395 cm<sup>-1</sup> for the 30012 $\leftarrow$ 00001 band), rather than independently measuring the half-width and pressureinduced shift coefficients for each spectral line in every spectrum and regressing these individual results to obtain the final coefficients. A modified multispectrum nonlinear least-squares retrieval procedure, including the capability to constrain spectral line parameters such as positions and intensities, enabled us to minimize the measurement uncertainties of the various retrieved parameters. Details of the retrieval algorithm will be provided in a separate article by Benner et al. [34].

### 2. Experimental

The experimental procedure has been described in [1–5]. All data were recorded at 0.01 cm<sup>-1</sup> resolution over the 3800–8500 cm<sup>-1</sup> range, using the McMath–Pierce Fourier transform spectrometer of the National Solar Observatory on Kitt Peak, Arizona. To ensure consistency with our previous work, the same 15 spectra used to determine  $CO_2$  self-broadening parameters in refs. 4 and 5 were included in the present analysis. These 15 spectra were recorded at

**Fig. 1.** Multispectrum fit of self- and Ar-broadened CO<sub>2</sub> spectra from 6280 to 6395 cm<sup>-1</sup>. (*a*) Twenty-one experimental spectra recorded at  $\sim 0.01$  cm<sup>-1</sup> resolution using the Fourier transform spectrometer at the National Solar Observatory on Kitt Peak. The set includes 15 highpurity CO<sub>2</sub> spectra in a natural mix of isotopologues and six CO<sub>2</sub> + Ar spectra recorded near room temperature. Positions of transitions included in the fit are indicated by tick marks shown at the top of panel (*a*). Each spectrum is normalized to the highest signal in the fitted interval. The 100% absorption line is shown by dotted line at the bottom of panel (*a*). (*b*) The corresponding weighted residuals (observed minus calculated on an expanded vertical scale) using a Voigt profile modified with speed dependence and line mixing (via relaxation matrix). (*c*) The weighted residuals for the six Ar-broadened CO<sub>2</sub> spectra. Panels (*b*) and (*c*) illustrate that appropriate weights were used for each of the 21 spectra in the analysis. The residuals shown in panel (*c*) are identical to the fit residuals for the six Ar-broadened spectra in (*b*) and are shown separately for illustrative purpose only.



room temperature ( $\sim 294$  K), with path lengths ranging from L = 2.46 to 49 m. The self-broadened spectra were augmented by six Ar-broadened CO<sub>2</sub> spectra, also recorded at room temperature, using the same experimental set up. The volume mixing ratios of CO<sub>2</sub> in the CO<sub>2</sub>–Ar spectra ranged from 0.05 to 0.09. Table 1 summarizes the experimental conditions for all spectra used in the present analysis.

# 3. Data retrieval and analysis

The multispectrum retrieval procedure used in the present work is the same used previously to determine accurate line positions, absolute intensities, self- and air-broadened halfwidth and pressure-shift coefficients, self and air line-mixing coefficients, and speed dependence for transitions up to J'' =60 in the 30012 $\leftarrow$ 00001 and 30013 $\leftarrow$ 00001 bands [4, 5].

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Lina	<b>D</b> ocition <sup><i>a</i></sup>	$b^0(\Lambda r)^b$	$\operatorname{Upp}(\mathbb{Z})$	$s^0(\Lambda r)^c$ upo	<b>SD</b> <sup>d</sup>	$\operatorname{Upp}(\mathcal{O}_{r})$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D62a	6 295 999 62	$\frac{D_L^{(AI)}}{0.041.76}$	6 30	$0^{\circ}(AI)^{\circ}$ unc.	0.1	Unc. (%)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	F020	6 200 650 27	0.041 70	0.39	-0.011 47 (200)	0.1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	P560	6 202 006 70	0.032 08	2.02	-0.013 15 (143) 0.007 76 (85)	0.1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D54e	6 292.990 79	0.047 03	1.05	-0.007 70 (83)	0.1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D520	6 293.319 70	0.048 17	0.88	$-0.010\ 15\ (39)$ $0.000\ 78\ (41)$	0.1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	P50e	6 200 803 14	0.047 47	0.88	-0.00978(41)	0.1	
$ \begin{array}{c} P46e & 6 302.172 & 0.5 & 0.059 & 11 & 0.36 & -0.009 & 10 & (17) & 0.1 \\ P44e & 6 306.565 & 25 & 0.051 & 102 & 0.27 & -0.008 & 86 & (13) & 0.1 \\ P42e & 6 308.737 & 56 & 0.051 & 48 & 0.21 & -0.008 & 81 & (10) & 0.1 \\ P36e & 6 313.002 & 45 & 0.052 & 19 & 0.15 & -0.008 & 81 & (10) & 0.094 & 1.7 \\ P36e & 6 315.094 & 37 & 0.052 & 88 & 0.13 & -0.008 & 30 & (7) & 0.093 & 1.6 \\ P32e & 6 319.195 & 68 & 0.054 & 0.2 & 0.11 & -0.008 & 37 & (7) & 0.003 & 1.6 \\ P32e & 6 312.204 & 52 & 0.054 & 22 & 0.11 & -0.008 & 37 & (7) & 0.105 & 1.3 \\ P34e & 6 312.1204 & 52 & 0.055 & 20 & 0.11 & -0.008 & 37 & (7) & 0.103 & 1.3 \\ P26e & 6 325.137 & 35 & 0.056 & 21 & 0.11 & -0.007 & 93 & (6) & 0.100 & 1.4 \\ P26e & 6 325.137 & 55 & 0.056 & 21 & 0.11 & -0.007 & 70 & (5) & 0.103 & 1.3 \\ P24e & 6 325.67 & 69 & 0.067 & 0.10 & -0.007 & 78 & (5) & 0.114 & 1.1 \\ P26e & 6 330.821 & 4 & 0.059 & 76 & 0.10 & -0.007 & 05 & 0.120 & 1.1 \\ P16e & 6 334.464 & 79 & 0.062 & 52 & 0.14 & -0.006 & 83 & (9) & 0.139 & 0.9 \\ P14e & 6 335.07 & 69 & 0.066 & 74 & 0.09 & -0.006 & 84 & (5) & 0.137 & 0.9 \\ P12e & 6 339.708 & 0.0665 & 59 & 0.09 & -0.006 & 80 & (5) & 0.138 & 0.8 \\ P10e & 6 343.055 & 10 & 0.070 & 66 & 0.17 & -0.005 & 40 & (12) & 0.122 & 1.0 \\ P08e & 6 341.397 & 01 & 0.068 & 80 & 0.10 & -0.006 & 20 & (6) & 0.134 & 0.9 \\ P10e & 6 344.684 & 03 & 0.072 & 91 & 0.14 & -0.005 & 20 & (10) & 0.122 & 1.0 \\ P08e & 6 341.397 & 01 & 0.068 & 80 & 0.10 & -0.006 & 20 & (6) & 0.134 & 0.9 \\ P06e & 6 343.055 & 10 & 0.070 & 65 & 0.18 & -0.004 & 15 & (17) & 0.129 & 1.0 \\ P08e & 6 341.397 & 01 & 0.068 & 50 & 0.9 & -0.006 & 316 & 0.122 & 1.0 \\ P08e & 6 345.382 & 0.080 & 52 & 0.31 & -0.002 & 632 & 0.100 & 2.1 \\ P02e & 6 344.684 & 03 & 0.072 & 91 & 0.14 & -0.005 & 92 & (10) & 0.122 & 1.0 \\ P04e & 6 344.684 & 03 & 0.079 & 70 & 11 & -0.004 & 33 & (8) & 0.118 & 1.1 \\ P02e & 6 362.537 & 0.058 & 50 & 0.9 & -0.006 & 32 & 0.100 & 2.1 \\ P02e & 6 362.537 & 0.058 & 0.22 & 0.31 & -0.006 & 32 & 0.100 & 2.1 \\ P02e & 6 364.628 & 0.00537 & 0.010 & -0.006 & 0.5 & 0.110 & 1.3 \\ P04e & 6 354.$	D180	6 202 142 65	0.048 78	0.04	$-0.011\ 02\ (30)$	0.1	
$ \begin{array}{c} 1.0c & 0.304, 50.6 & 0.50 & 0.051 & 0.27 & -0.008 & 81 (10) & 0.1 \\ 1.0c & 0.306, 565 & 25 & 0.051 & 48 & 0.21 & -0.008 & 81 (10) & 0.1 \\ 1.0c & 0.310, 833 & 00 & 0.051 & 93 & 0.17 & -0.008 & 88 (0.10) & 0.094 & 1.7 \\ 1.0c & 0.310, 802 & 45 & 0.052 & 19 & 0.15 & -0.008 & 81 (00) & 0.094 & 1.7 \\ 1.0c & 0.311, 158 & 70 & 0.052 & 88 & 0.13 & -0.008 & 30 (70) & 0.093 & 1.6 \\ 1.0c & 0.311, 158 & 70 & 0.053 & 24 & 0.13 & -0.008 & 30 (70) & 0.093 & 1.6 \\ 1.0c & 0.311, 158 & 70 & 0.053 & 24 & 0.13 & -0.008 & 30 (70) & 0.093 & 1.6 \\ 1.0c & 0.321, 851 & 68 & 0.054 & 02 & 0.11 & -0.008 & 37 (7) & 0.105 & 1.3 \\ 1.0c & 0.321, 851 & 60 & 0.055 & 20 & 0.11 & -0.007 & 93 (60 & 0.100 & 1.4 \\ 1.266 & 6325, 137 & 35 & 0.056 & 21 & 0.11 & -0.007 & 70 (5) & 0.103 & 1.3 \\ 1.266 & 6325, 137 & 35 & 0.056 & 21 & 0.11 & -0.007 & 70 (5) & 0.103 & 1.3 \\ 1.266 & 6326, 120 & 0.057 & 76 & 0.10 & -0.007 & 78 (5) & 0.114 & 1.1 \\ 1.206 & 6330, 821 & 24 & 0.059 & 76 & 0.10 & -0.007 & 78 (5) & 0.114 & 1.1 \\ 1.206 & 6332, 637 & 0.060 & 74 & 0.10 & -0.007 & 78 (5) & 0.127 & 0.9 \\ 1.26 & 6332, 903 & 60 & 0.065 & 79 & 0.09 & -0.006 & 84 (5) & 0.137 & 0.9 \\ 1.26 & 6337, 903 & 60 & 0.066 & 74 & 0.09 & -0.006 & 84 (5) & 0.137 & 0.9 \\ 1.26 & 6337, 903 & 60 & 0.066 & 74 & 0.09 & -0.006 & 02 (6) & 0.124 & 1.0 \\ 1.06 & 0.344, 464 & 30 & 0.072 & 91 & 0.14 & -0.005 & 92 (10) & 0.112 & 1.2 \\ 1.06 & 0.344, 628 & 0.070 & 85 & 0.18 & -0.004 & 15 (17) & 0.129 & 1.0 \\ 1.06 & 634, 638 & 0.070 & 65 & 0.18 & -0.004 & 30 (12) & 0.121 & 1.0 \\ 1.06 & 0.344, 623 & 0.070 & 85 & 0.18 & -0.004 & 30 (12) & 0.121 & 1.0 \\ 1.06 & 0.350, 133 & 0.068 & 94 & 0.19 & -0.006 & 26 (32) & 0.100 & 2.1 \\ 1.00 & 0.06 & 6351, 133 & 0.068 & 94 & 0.19 & -0.004 & 30 (12) & 0.122 & 1.0 \\ 1.00 & 0.46 & 6351, 60 & 15 & 0.070 & 7 & 0.104 & -0.005 & 50 (6) & 0.129 & 1.0 \\ 1.00 & 0.350 & 31 & 0.007 & 0.55 & 0.18 & -0.007 & 16 & 0.128 & 1.0 \\ 1.00 & 0.350 & 31 & 0.007 & 0.55 & 0.18 & -0.007 & 31 (5) & 0.129 & 1.0 \\ 1.10 & 0.06 & 6351, 323 & 0.100 & -0.006 & 50 (5) & 0.110 & 1.3 \\ 1.10 & 0.06 $	Г40C D46a	6 304 366 82	0.049 /1	0.40	$-0.008\ 00\ (22)$ $0.000\ 10\ (17)$	0.1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D440C	6 306 565 25	0.050 17	0.30	$-0.009\ 10\ (17)$	0.1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D/20	6 308 737 56	0.051.02	0.27	$-0.008 \ 81 \ (10)$	0.1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	P40e	6 310 883 40	0.051.03	0.21	-0.008 81 (10)	0.1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D380	6 313 002 45	0.052 10	0.17	-0.008 + 0(0)	0.1	17
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D360	6 315 004 37	0.052.89	0.13	$-0.008 \ 30 \ (10)$	0.094	1.7
	P3/1e	6 317 158 87	0.052 88	0.13	$-0.008 \ 31 \ (8)$ $0.008 \ 30 \ (7)$	0.089	1.6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D320	6 310 105 68	0.053 24	0.13	$-0.008 \ 30 \ (7)$	0.093	1.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D30e	6 321 204 52	0.054 02	0.11	$-0.008 \ 37 \ (7)$	0.105	1.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D280	6 323 185 16	0.054 25	0.11	$-0.008\ 13\ (0)$	0.085	1.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 200 P26e	6 325 137 35	0.055 20	0.11	-0.00793(0)	0.100	1.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D240	6 327 060 00	0.057.06	0.11	-0.008 01 (5)	0.103	1.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P22e	6 328 955 59	0.057 00	0.11	-0.007 70 (3)	0.105	1.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P20e	6 330 821 24	0.050 76	0.10	-0.007  38  (5)	0.127	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P18e	6 332 657 69	0.059 70	0.10	-0.007 + 3(5)	0.127	1.1
P14e       6 336.424 73       0.002 32       0.14       -0.006 83 (5)       0.137       0.9         P12e       6 337.990 36       0.065 59       0.09       -0.006 84 (5)       0.138       0.8         P10e       6 339.708 60       0.066 74       0.09       -0.006 84 (5)       0.134       0.9         P08e       6 341.397 01       0.068 80       0.10       -0.006 40 (12)       0.121       1.0         P06e       6 343.055 51       0.070 66       0.17       -0.005 40 (12)       0.112       1.2         P02e       6 346.282 51       0.076 85       0.18       -0.002 63 (32)       0.100       2.1         R02e       6 350.147 05       0.074 21       0.13       -0.004 39 (12)       0.122       1.0         R04e       6 351.103 13       0.068 94       0.19       -0.004 30 (6)       0.124       1.0         R04e       6 355.938 80       0.065 36       0.09       -0.004 33 (5)       0.127       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.004 33 (5)       0.127       1.0         R12e       6 356.54 38       0.062 02       0.11       -0.005 57 (6)       0.126       1.0         R12e       6 362.503 79	P16e	6 334 464 79	0.062 52	0.10	$-0.007 \ 03 \ (3)$	0.120	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P1/e	6 336 242 38	0.063.94	0.09	$-0.000\ 85\ (5)$	0.137	0.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D12e	6 337 990 36	0.065 59	0.09	$-0.000 \ 80 \ (5)$	0.137	0.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P10e	6 339 708 60	0.065 74	0.09	-0.006 25 (6)	0.125	1.0
Note0 3 11 0 3 0 3 0 3 0 3 0 1 0 3 0 3 0 3 0	P08e	6 341 397 01	0.068 80	0.09	-0.006 02 (6)	0.125	0.9
Note0 3 10 100 000.0110.000 1000.1121.0P04e6 344.684 030.072 910.14-0.005 92 (10)0.1121.2P02e6 346.282 510.076 850.18-0.004 15 (17)0.1291.0R00e6 348.623 820.080 520.31-0.002 63 (32)0.1002.1R02e6 350.147 050.074 210.13-0.004 39 (12)0.1221.0R04e6 351.640 150.070 970.11-0.004 33 (8)0.1181.1R06e6 353.103 130.068 940.19-0.004 81 (12)0.1231.0R08e6 354.536 000.066 770.10-0.004 95 (6)0.1291.0R12e6 357.311 570.063 650.09-0.005 57 (6)0.1261.0R14e6 358.654 380.062 020.11-0.006 00 (5)0.1101.3R18e6 361.250 400.059 740.10-0.006 26 (5)0.1151.2R20e6 362.503 790.058 230.10-0.006 26 (5)0.1101.3R18e6 361.270 f10.057 180.12-0.006 82 (7)0.1091.4R24e6 364.921 970.056 160.11-0.007 01 (6)0.1061.5R26e6 366.087 030.055 310.11-0.007 22 (7)0.1041.6R30e6 368.329 890.053 700.11-0.007 22 (7)0.1041.6R32e6 369.408 070.053 080.13-0.007 89 (7)0.090 1.9 <t< td=""><td>P06e</td><td>6 343 055 51</td><td>0.070.66</td><td>0.10</td><td>-0.005 40 (12)</td><td>0.121</td><td>1.0</td></t<>	P06e	6 343 055 51	0.070.66	0.10	-0.005 40 (12)	0.121	1.0
PO2e       6 346.282 51       0.076 85       0.11       -0.004 15 (17)       0.129       1.0         R00e       6 348.623 82       0.080 52       0.31       -0.002 63 (32)       0.100       2.1         R02e       6 350.147 05       0.074 21       0.13       -0.004 39 (12)       0.122       1.0         R04e       6 351.640 15       0.070 97       0.11       -0.004 33 (8)       0.118       1.1         R06e       6 353.103 13       0.068 94       0.19       -0.004 70 (6)       0.124       1.0         R10e       6 355.938 80       0.065 36       0.09       -0.004 95 (6)       0.129       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.005 33 (5)       0.127       1.0         R14e       6 358.654 38       0.062 02       0.11       -0.005 57 (6)       0.126       1.0         R16e       6 361.250 40       0.059 74       0.10       -0.006 31 (5)       0.110       1.3         R18e       6 364.921 97       0.058 12       0.100       -0.006 32 (5)       0.110       1.4         R22e       6 366.87 03       0.055 31       0.11       -0.006 42 (6)       0.102       1.6         R24e       6 364.921 97	P04e	6 344 684 03	0.072 91	0.17	$-0.005 \ 92 \ (10)$	0.121	1.0
Robe6 348.623 820.080 520.13-0.004 39 (12)0.1002.1R02e6 350.147 050.074 210.13-0.004 39 (12)0.1221.0R04e6 351.640 150.070 970.11-0.004 33 (8)0.1181.1R06e6 353.103 130.068 940.19-0.004 81 (12)0.1231.0R08e6 354.536 000.066 770.10-0.004 70 (6)0.1241.0R12e6 355.938 800.065 360.09-0.004 95 (6)0.1291.0R14e6 358.654 380.062 020.11-0.005 57 (6)0.1261.0R14e6 358.654 380.062 020.11-0.006 00 (5)0.1101.3R18e6 361.250 400.059 740.10-0.006 26 (5)0.1151.2R20e6 362.503 790.058 230.10-0.006 31 (5)0.1091.4R22e6 363.727 610.057 180.12-0.006 82 (7)0.1091.4R24e6 364.921 970.056 160.11-0.007 27 (6)0.0931.8R32e6 367.222 940.054 540.13-0.007 27 (6)0.0931.8R32e6 369.408 070.053 080.13-0.007 89 (7)0.0901.9R34e6 370.457 700.052 650.25-0.008 10 (12)0.1171.5R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R42e6 374.375 490.050 880.22-0.008 53 (12)0	P02e	6 346 282 51	0.076.85	0.11	$-0.003 \ 15 \ (17)$	0.129	1.2
R02e       6 350.147 05       0.074 21       0.13       -0.004 39 (12)       0.122       1.0         R04e       6 351.640 15       0.070 97       0.11       -0.004 33 (8)       0.118       1.1         R06e       6 353.103 13       0.068 94       0.19       -0.004 81 (12)       0.123       1.0         R08e       6 354.536 00       0.066 77       0.10       -0.004 70 (6)       0.124       1.0         R10e       6 355.938 80       0.065 36       0.09       -0.004 95 (6)       0.129       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.005 57 (6)       0.126       1.0         R14e       6 359.967 29       0.060 70       0.10       -0.006 05       0.110       1.3         R18e       6 361.250 40       0.059 74       0.10       -0.006 26 (5)       0.115       1.2         R20e       6 362.503 79       0.058 23       0.10       -0.006 82 (7)       0.109       1.4         R22e       6 366.87 03       0.055 31       0.11       -0.006 94 (6)       0.102       1.6         R26e       6 366.087 03       0.055 31       0.11       -0.007 22 (7)       0.104       1.6         R30e       6 368.329 89	R00e	6 348 623 82	0.080.52	0.10	-0.002.63(32)	0.100	2.1
R04c       6 351.640 15       0.070 97       0.11       -0.004 33 (8)       0.118       1.1         R06e       6 353.103 13       0.068 94       0.19       -0.004 33 (8)       0.118       1.1         R06e       6 354.536 00       0.066 77       0.10       -0.004 70 (6)       0.124       1.0         R10e       6 355.938 80       0.065 36       0.09       -0.004 95 (6)       0.129       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.005 57 (6)       0.126       1.0         R14e       6 359.967 29       0.060 70       0.10       -0.006 26 (5)       0.115       1.2         R20e       6 361.250 40       0.059 74       0.10       -0.006 26 (5)       0.115       1.2         R20e       6 362.503 79       0.058 23       0.10       -0.006 82 (7)       0.109       1.4         R22e       6 366.77 61       0.057 18       0.12       -0.006 82 (7)       0.109       1.4         R24e       6 366.087 03       0.055 31       0.11       -0.007 01 (6)       0.106       1.5         R28e       6 367.222 94       0.054 54       0.13       -0.007 22 (7)       0.104       1.6         R30e       6 368.329 89 <td>R02e</td> <td>6 350 147 05</td> <td>0.074 21</td> <td>0.13</td> <td>-0.002 39 (32)</td> <td>0.122</td> <td>1.0</td>	R02e	6 350 147 05	0.074 21	0.13	-0.002 39 (32)	0.122	1.0
R06e       6 353.103 13       0.068 94       0.19       -0.004 81 (12)       0.123       1.0         R08e       6 354.536 00       0.066 77       0.10       -0.004 70 (6)       0.124       1.0         R10e       6 355.938 80       0.065 36       0.09       -0.004 95 (6)       0.129       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.005 57 (6)       0.126       1.0         R14e       6 358.654 38       0.062 02       0.11       -0.006 00 (5)       0.110       1.3         R16e       6 359.967 29       0.060 70       0.10       -0.006 26 (5)       0.115       1.2         R20e       6 362.503 79       0.058 23       0.10       -0.006 82 (7)       0.109       1.4         R22e       6 364.921 97       0.056 16       0.11       -0.007 01 (6)       0.106       1.5         R24e       6 364.921 97       0.055 31       0.11       -0.007 01 (6)       0.106       1.5         R28e       6 367.222 94       0.054 54       0.13       -0.007 22 (7)       0.104       1.6         R30e       6 368.329 89       0.053 70       0.11       -0.007 27 (6)       0.093       1.8         R32e       6 369.408 07 </td <td>R04e</td> <td>6 351.640 15</td> <td>0.070 97</td> <td>0.11</td> <td>-0.004 33 (8)</td> <td>0.118</td> <td>1.1</td>	R04e	6 351.640 15	0.070 97	0.11	-0.004 33 (8)	0.118	1.1
R08e       6 354.536 00       0.065 77       0.10       -0.004 70 (6)       0.129       1.0         R10e       6 355.938 80       0.065 36       0.09       -0.004 95 (6)       0.129       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.005 33 (5)       0.127       1.0         R14e       6 358.654 38       0.062 02       0.11       -0.005 57 (6)       0.126       1.0         R16e       6 359.967 29       0.060 70       0.10       -0.006 00 (5)       0.110       1.3         R18e       6 361.250 40       0.059 74       0.10       -0.006 26 (5)       0.115       1.2         R20e       6 362.503 79       0.058 23       0.10       -0.006 82 (7)       0.109       1.4         R22e       6 364.921 97       0.056 16       0.11       -0.006 94 (6)       0.102       1.6         R26e       6 367.222 94       0.054 54       0.13       -0.007 22 (7)       0.104       1.6         R30e       6 368.329 89       0.053 70       0.11       -0.007 89 (7)       0.090       1.9         R34e       6 370.457 70       0.052 69       0.13       -0.008 17 (8)       0.084       2.3         R36e       6 371.478 99 <td>R06e</td> <td>6 353 103 13</td> <td>0.068 94</td> <td>0.19</td> <td><math>-0.004 \ 81 \ (12)</math></td> <td>0.123</td> <td>1.0</td>	R06e	6 353 103 13	0.068 94	0.19	$-0.004 \ 81 \ (12)$	0.123	1.0
R10c       6 355.938 80       0.065 36       0.09       -0.004 95 (6)       0.129       1.0         R12e       6 357.311 57       0.063 65       0.09       -0.005 33 (5)       0.127       1.0         R14e       6 358.654 38       0.062 02       0.11       -0.005 57 (6)       0.126       1.0         R16e       6 359.967 29       0.060 70       0.10       -0.006 00 (5)       0.110       1.3         R18e       6 361.250 40       0.059 74       0.10       -0.006 26 (5)       0.115       1.2         R20e       6 362.503 79       0.058 23       0.10       -0.006 82 (7)       0.109       1.4         R22e       6 363.727 61       0.057 18       0.12       -0.006 82 (7)       0.109       1.4         R24e       6 364.921 97       0.056 16       0.11       -0.007 01 (6)       0.106       1.5         R28e       6 367.222 94       0.054 54       0.13       -0.007 22 (7)       0.104       1.6         R30e       6 368.329 89       0.053 70       0.11       -0.007 89 (7)       0.090       1.9         R34e       6 370.457 70       0.052 69       0.13       -0.008 17 (8)       0.084       2.3         R36e       6 371.478 99 <td>R08e</td> <td>6 354.536 00</td> <td>0.066 77</td> <td>0.10</td> <td>-0.004 70 (6)</td> <td>0.124</td> <td>1.0</td>	R08e	6 354.536 00	0.066 77	0.10	-0.004 70 (6)	0.124	1.0
R12e6 357.311 570.063 650.09 $-0.005 33 (5)$ 0.1271.0R14e6 358.654 380.062 020.11 $-0.005 57 (6)$ 0.1261.0R16e6 359.967 290.060 700.10 $-0.006 00 (5)$ 0.1101.3R18e6 361.250 400.059 740.10 $-0.006 26 (5)$ 0.1151.2R20e6 362.503 790.058 230.10 $-0.006 31 (5)$ 0.1091.4R22e6 363.727 610.057 180.12 $-0.006 82 (7)$ 0.1091.4R24e6 364.921 970.056 160.11 $-0.007 01 (6)$ 0.1061.5R28e6 367.222 940.054 540.13 $-0.007 22 (7)$ 0.1041.6R30e6 368.329 890.053 700.11 $-0.007 89 (7)$ 0.0901.9R34e6 370.457 700.052 690.13 $-0.008 17 (8)$ 0.0842.3R36e6 371.478 990.052 650.25 $-0.008 10 (12)$ 0.1171.5R38e6 372.472 210.051 140.18 $-0.007 85 (11)$ 0.0832.6R40e6 373.437 620.051 370.19 $-0.008 53 (12)$ 0.1111.5R42e6 376.169 890.049 860.52 $-0.009 28 (24)$ 0.1R44e6 375.286 140.049 960.28 $-0.009 28 (24)$ 0.1R44e6 377.027 070.048 910.49 $-0.009 78 (23)$ 0.1R48e6 377.027 070.048 910.49 $-0.010 02 (30)$ 0.1	R10e	6 355.938 80	0.065 36	0.09	-0.004 95 (6)	0.129	1.0
R14e6 358.654 380.062 020.11 $-0.005 57 (6)$ 0.1261.0R16e6 359.967 290.060 700.10 $-0.006 00 (5)$ 0.1101.3R18e6 361.250 400.059 740.10 $-0.006 26 (5)$ 0.1151.2R20e6 362.503 790.058 230.10 $-0.006 31 (5)$ 0.1091.4R22e6 363.727 610.057 180.12 $-0.006 82 (7)$ 0.1091.4R24e6 364.921 970.056 160.11 $-0.007 01 (6)$ 0.1021.6R26e6 366.087 030.055 310.11 $-0.007 22 (7)$ 0.1041.6R30e6 368.329 890.053 700.11 $-0.007 22 (7)$ 0.1041.6R32e6 369.408 070.052 690.13 $-0.007 89 (7)$ 0.0901.9R34e6 370.457 700.052 690.13 $-0.008 17 (8)$ 0.0842.3R36e6 371.478 990.052 650.25 $-0.008 10 (12)$ 0.1171.5R38e6 372.472 210.051 140.18 $-0.007 85 (11)$ 0.0832.6R40e6 373.437 620.051 370.19 $-0.008 53 (10)$ 0.111R42e6 376.169 890.049 860.52 $-0.009 28 (24)$ 0.1R44e6 377.027 070.048 910.49 $-0.009 78 (23)$ 0.1R48e6 377.027 070.048 910.49 $-0.010 02 (30)$ 0.1	R12e	6 357.311 57	0.063 65	0.09	-0.005 33 (5)	0.127	1.0
R16e6 359.967 290.060 700.10-0.006 00 (5)0.1101.3R18e6 361.250 400.059 740.10-0.006 26 (5)0.1151.2R20e6 362.503 790.058 230.10-0.006 31 (5)0.1091.4R22e6 363.727 610.057 180.12-0.006 82 (7)0.1091.4R24e6 364.921 970.056 160.11-0.006 94 (6)0.1021.6R26e6 366.087 030.055 310.11-0.007 01 (6)0.1061.5R28e6 367.222 940.054 540.13-0.007 22 (7)0.1041.6R30e6 368.329 890.053 700.11-0.007 89 (7)0.0901.9R34e6 370.457 700.052 690.13-0.007 89 (7)0.0901.9R34e6 371.478 990.052 650.25-0.008 10 (12)0.1171.5R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 376.169 890.049 960.28-0.009 20 (13)0.11R46e6 376.169 890.049 860.52-0.009 78 (23)0.11R48e6 377.027 070.048 910.49-0.009 78 (23)0.11R48e6 377.858 060.048 150.64-0.010 02 (30)0.1	R14e	6 358.654 38	0.062 02	0.11	-0.005 57 (6)	0.126	1.0
R18e $6\ 361.250\ 40$ $0.059\ 74$ $0.10$ $-0.006\ 26\ (5)$ $0.115$ $1.2$ R20e $6\ 362.503\ 79$ $0.058\ 23$ $0.10$ $-0.006\ 31\ (5)$ $0.109$ $1.4$ R22e $6\ 363.727\ 61$ $0.057\ 18$ $0.12$ $-0.006\ 82\ (7)$ $0.109$ $1.4$ R24e $6\ 364.921\ 97$ $0.056\ 16$ $0.11$ $-0.006\ 82\ (7)$ $0.109$ $1.4$ R26e $6\ 366.087\ 03$ $0.055\ 31$ $0.11$ $-0.006\ 94\ (6)$ $0.102$ $1.6$ R26e $6\ 366.087\ 03$ $0.055\ 31$ $0.11$ $-0.007\ 01\ (6)$ $0.106\ 1.5$ R28e $6\ 367.222\ 94$ $0.054\ 54$ $0.13$ $-0.007\ 22\ (7)$ $0.104\ 1.6$ R30e $6\ 368.329\ 89$ $0.053\ 70$ $0.11$ $-0.007\ 27\ (6)$ $0.093\ 1.8$ R32e $6\ 369.408\ 07$ $0.052\ 69$ $0.13\ -0.007\ 89\ (7)$ $0.090\ 1.9$ R34e $6\ 370.457\ 70$ $0.052\ 69\ 0.13\ -0.007\ 89\ (7)$ $0.090\ 1.9$ R34e $6\ 371.478\ 99\ 0.052\ 65\ 0.25\ -0.008\ 10\ (12)\ 0.117\ 1.5$ R38e $6\ 372.472\ 21\ 0.051\ 14\ 0.18\ -0.007\ 85\ (11)\ 0.083\ 2.6$ R40e $6\ 373.437\ 62\ 0.051\ 37\ 0.19\ -0.008\ 53\ (12)\ 0.111\ 1.5$ R42e $6\ 374.375\ 49\ 0.050\ 88\ 0.22\ -0.008\ 53\ (10)\ 0.1$ R44e $6\ 375.286\ 14\ 0.049\ 96\ 0.28\ -0.009\ 28\ (24)\ 0.1$ R46e $6\ 377.027\ 07\ 0.048\ 91\ 0.49\ -0.009\ 78\ (23)\ 0.1$ R48e $6\ 377.858\ 06\ 0.048\ 15\ 0.64\ -0.010\ 02\ (30)\ 0.1$	R16e	6 359.967 29	0.060 70	0.10	-0.006 00 (5)	0.110	1.3
R20e $6\ 362.503\ 79$ $0.058\ 23$ $0.10$ $-0.006\ 31$ (5) $0.109$ $1.4$ R22e $6\ 363.727\ 61$ $0.057\ 18$ $0.12$ $-0.006\ 82\ (7)$ $0.109$ $1.4$ R24e $6\ 364.921\ 97$ $0.056\ 16$ $0.11$ $-0.006\ 94\ (6)$ $0.102$ $1.6$ R26e $6\ 366.087\ 03$ $0.055\ 31$ $0.11$ $-0.007\ 01\ (6)$ $0.106\ 1.5$ R28e $6\ 367.222\ 94$ $0.054\ 54$ $0.13$ $-0.007\ 22\ (7)$ $0.104\ 1.6$ R30e $6\ 368.329\ 89$ $0.053\ 70$ $0.11\ -0.007\ 27\ (6)$ $0.093\ 1.8$ R32e $6\ 369.408\ 07$ $0.052\ 69\ 0.13$ $-0.007\ 89\ (7)$ $0.090\ 1.9$ R34e $6\ 370.457\ 70$ $0.052\ 69\ 0.13$ $-0.008\ 17\ (8)$ $0.084\ 2.3$ R36e $6\ 371.478\ 99\ 0.052\ 65\ 0.25$ $-0.008\ 10\ (12)\ 0.117\ 1.5$ R38e $6\ 372.472\ 21\ 0.051\ 14\ 0.18\ -0.007\ 85\ (11)\ 0.083\ 2.6$ R40e $6\ 373.437\ 62\ 0.051\ 37\ 0.19\ -0.008\ 53\ (12)\ 0.111\ 1.5$ R42e $6\ 374.375\ 49\ 0.050\ 88\ 0.22\ -0.008\ 53\ (10)\ 0.1$ R44e $6\ 375.286\ 14\ 0.049\ 96\ 0.28\ -0.009\ 20\ (13)\ 0.1$ R46e $6\ 377.027\ 07\ 0.048\ 91\ 0.49\ -0.009\ 78\ (23)\ 0.1$ R48e $6\ 377.858\ 06\ 0.048\ 15\ 0.64\ -0.010\ 02\ (30)\ 0.1$	R18e	6 361.250 40	0.059 74	0.10	-0.006 26 (5)	0.115	1.2
R22e $6\ 363.727\ 61$ $0.057\ 18$ $0.12$ $-0.006\ 82\ (7)$ $0.109$ $1.4$ R24e $6\ 364.921\ 97$ $0.056\ 16$ $0.11$ $-0.006\ 94\ (6)$ $0.102$ $1.6$ R26e $6\ 366.087\ 03$ $0.055\ 31$ $0.11$ $-0.007\ 01\ (6)$ $0.106$ $1.5$ R28e $6\ 367.222\ 94$ $0.054\ 54$ $0.13$ $-0.007\ 22\ (7)$ $0.104$ $1.6$ R30e $6\ 368.329\ 89$ $0.053\ 70$ $0.11$ $-0.007\ 22\ (7)$ $0.104$ $1.6$ R32e $6\ 369.408\ 07$ $0.053\ 08$ $0.13$ $-0.007\ 27\ (6)$ $0.093$ $1.8$ R32e $6\ 369.408\ 07$ $0.052\ 69$ $0.13$ $-0.007\ 89\ (7)$ $0.090\ 1.9$ R34e $6\ 370.457\ 70$ $0.052\ 69$ $0.13$ $-0.008\ 17\ (8)$ $0.084\ 2.3$ R36e $6\ 371.478\ 99$ $0.052\ 65$ $0.25$ $-0.008\ 10\ (12)$ $0.117\ 1.5$ R38e $6\ 372.472\ 21$ $0.051\ 14$ $0.18\ -0.007\ 85\ (11)$ $0.083\ 2.6$ R40e $6\ 374.375\ 49$ $0.050\ 88\ 0.22\ -0.008\ 53\ (10)$ $0.1\ 111\ 1.5$ R42e $6\ 376.169\ 89\ 0.049\ 96\ 0.28\ -0.009\ 20\ (13)$ $0.1\ 111\ 1.5$ R46e $6\ 377.027\ 07\ 0.048\ 91\ 0.49\ -0.007\ 78\ (23)$ $0.1\ 111\ 1.5$ R48e $6\ 377.858\ 06\ 0.048\ 15\ 0.64\ -0.010\ 02\ (30)$ $0.1\ 111\ 1.5\ 1.5\ 111\ 1.5\ 1.5\ 1.5\ 1$	R20e	6 362.503 79	0.058 23	0.10	-0.006 31 (5)	0.109	1.4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R22e	6 363.727 61	0.057 18	0.12	-0.006 82 (7)	0.109	1.4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R24e	6 364.921 97	0.056 16	0.11	-0.006 94 (6)	0.102	1.6
R28e $6\ 367.222\ 94$ $0.054\ 54$ $0.13$ $-0.007\ 22\ (7)$ $0.104$ $1.6$ R30e $6\ 368.329\ 89$ $0.053\ 70$ $0.11$ $-0.007\ 22\ (7)$ $0.104$ $1.6$ R32e $6\ 369.408\ 07$ $0.053\ 08$ $0.13$ $-0.007\ 27\ (6)$ $0.093$ $1.8$ R32e $6\ 369.408\ 07$ $0.053\ 08$ $0.13$ $-0.007\ 27\ (6)$ $0.090$ $1.9$ R34e $6\ 370.457\ 70$ $0.052\ 69$ $0.13$ $-0.008\ 17\ (8)$ $0.084$ $2.3$ R36e $6\ 371.478\ 99$ $0.052\ 65$ $0.25$ $-0.008\ 10\ (12)$ $0.117$ $1.5$ R38e $6\ 372.472\ 21$ $0.051\ 14$ $0.18$ $-0.007\ 85\ (11)$ $0.083$ $2.6$ R40e $6\ 373.437\ 62$ $0.051\ 37$ $0.19$ $-0.008\ 53\ (12)$ $0.111$ $1.5$ R42e $6\ 374.375\ 49$ $0.050\ 88$ $0.22$ $-0.008\ 53\ (10)$ $0.1$ R44e $6\ 375.286\ 14$ $0.049\ 96$ $0.28$ $-0.009\ 20\ (13)$ $0.1$ R46e $6\ 377.027\ 07$ $0.048\ 91$ $0.49$ $-0.009\ 78\ (23)$ $0.1$ R48e $6\ 377.858\ 06$ $0.048\ 15$ $0.64$ $-0.010\ 02\ (30)$ $0.1$	R26e	6 366.087 03	0.055 31	0.11	-0.007 01 (6)	0.106	1.5
R30e6 368.329 890.053 700.11-0.007 27 (6)0.0931.8R32e6 369.408 070.053 080.13-0.007 89 (7)0.0901.9R34e6 370.457 700.052 690.13-0.008 17 (8)0.0842.3R36e6 371.478 990.052 650.25-0.008 10 (12)0.1171.5R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R28e	6 367.222 94	0.054 54	0.13	-0.007 22 (7)	0.104	1.6
R32e6 369.408 070.053 080.13-0.007 89 (7)0.0901.9R34e6 370.457 700.052 690.13-0.008 17 (8)0.0842.3R36e6 371.478 990.052 650.25-0.008 10 (12)0.1171.5R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 78 (23)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R30e	6 368.329 89	0.053 70	0.11	-0.007 27 (6)	0.093	1.8
R34e6 370.457 700.052 690.13-0.008 17 (8)0.0842.3R36e6 371.478 990.052 650.25-0.008 10 (12)0.1171.5R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R32e	6 369.408 07	0.053 08	0.13	-0.007 89 (7)	0.090	1.9
R36e6 371.478 990.052 650.25-0.008 10 (12)0.1171.5R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R34e	6 370.457 70	0.052 69	0.13	-0.008 17 (8)	0.084	2.3
R38e6 372.472 210.051 140.18-0.007 85 (11)0.0832.6R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R36e	6 371.478 99	0.052 65	0.25	-0.008 10 (12)	0.117	1.5
R40e6 373.437 620.051 370.19-0.008 53 (12)0.1111.5R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R38e	6 372.472 21	0.051 14	0.18	-0.007 85 (11)	0.083	2.6
R42e6 374.375 490.050 880.22-0.008 53 (10)0.1R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R40e	6 373.437 62	0.051 37	0.19	-0.008 53 (12)	0.111	1.5
R44e6 375.286 140.049 960.28-0.009 20 (13)0.1R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R42e	6 374.375 49	0.050 88	0.22	-0.008 53 (10)	0.1	
R46e6 376.169 890.049 860.52-0.009 28 (24)0.1R48e6 377.027 070.048 910.49-0.009 78 (23)0.1R50e6 377.858 060.048 150.64-0.010 02 (30)0.1	R44e	6 375.286 14	0.049 96	0.28	-0.009 20 (13)	0.1	
R48e         6 377.027 07         0.048 91         0.49         -0.009 78 (23)         0.1           R50e         6 377.858 06         0.048 15         0.64         -0.010 02 (30)         0.1	R46e	6 376.169 89	0.049 86	0.52	-0.009 28 (24)	0.1	
R50e 6 377.858 06 0.048 15 0.64 -0.010 02 (30) 0.1	R48e	6 377.027 07	0.048 91	0.49	-0.009 78 (23)	0.1	
	R50e	6 377.858 06	0.048 15	0.64	-0.010 02 (30)	0.1	

**Table 2.** Ar-broadened half-width and pressure-induced shift coefficients and speed dependence in the  $30012 \leftarrow 00001$  band of  ${}^{16}O^{12}C^{16}O$ .

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Line	Position <sup>a</sup>	$b_L^0(\operatorname{Ar})^b$	Unc. (%)	$\delta^0(\operatorname{Ar})^c$ unc.	$\mathrm{SD}^d$	Unc. (%)
R52e	6 378.663 24	0.048 65	1.15	-0.011 38 (54)	0.1	
R54e	6 379.443 02	0.047 72	1.30	-0.009 58 (60)	0.1	
R56e	6 380.197 83	0.042 49	3.22	-0.010 09 (133)	0.1	
R58e	6 380.928 12	0.049 67	3.26	-0.009 64 (157)	0.1	

<sup>*a*</sup>Zero pressure line center positions are in  $cm^{-1}$ . While the position values were adjusted during the present study, to the accuracy given here they are the same as in [4]. See text for details.

<sup>b</sup>The measured Ar-broadened half-width coefficients are in cm<sup>-1</sup>/atm at 296 K.

<sup>c</sup>The measured Ar-induced pressure-shift coefficients are in cm<sup>-1</sup>/atm at the temperature of the spectra ( $\sim 294$  K;

see Table 1).

<sup>d</sup>Speed-dependence (SD) parameter (unitless).

The multispectrum retrieval constrained the line positions and line intensities of the fitted bands to well-known quantum mechanical expressions, so that spectroscopic parameters such as the rovibrational constants (G, B, D, H, ...) and intensities (band intensities and Herman-Wallis factors) are determined directly from the whole band analysis rather than determining individual line positions and line intensities, from which the various constants are determined [34]. In contrast, the multispectrum algorithm adjusted the half-width and the pressure-shift coefficient for each measured transition individually in the least-squares fits. In the present study, we used the same set of self-broadened spectra used in [4, 5] to ensure the same level of accuracy for the retrieved Ar-broadened half-widths, pressure shifts, and line mixing coefficients. Line positions, intensities, selfbroadened half-width, self-shift, and the off-diagonal relaxation matrix element coefficients for self-line mixing were fixed to values derived from the previous analyses [4, 5]. The parameters floated in the present study are the Arbroadened half-width and Ar pressure-induced shift, the offdiagonal relaxation matrix element coefficients due to Arbroadening for each measured line (or between a pair of lines for line mixing) in the  $30012 \leftarrow 00001$  and  $30013 \leftarrow$ 00001 bands. We have used a single speed dependence parameter for each line in the multispectrum fit; thus, this parameter includes concentration weighted contributions from both CO<sub>2</sub> and Ar.

The widely used convenient, approximate expressions, used for retrieving the pressure-broadened half-width and pressure-induced shift coefficients are given below,

$$b_{\rm L}(p,T) = p \left[ b_{\rm L}^0({\rm Ar})(p_0,T_0)(1-\chi) \left(\frac{T_0}{T}\right)^{n_1} + b_{\rm L}^0({\rm self})(p_0,T_0)\chi \left(\frac{T_0}{T}\right)^{n_2} \right] \quad (1)$$

$$\nu = \nu_0 + p[\delta^0(\operatorname{Ar})(1-\chi) + \delta^0(\operatorname{self})\chi]$$
(2)

$$\delta^{0}(T) = \delta^{0}(T_{0}) + \delta'(T - T_{0})$$
(3)

In (1)–(3), the reference pressure  $p_0 = 1$  atm, the temperature  $T_0 = 296$  K,  $b_{\rm L}^0$  and  $\delta^0$  represent the Lorentz pressurebroadened half-width (in cm<sup>-1</sup>/atm at 296 K) and pressure—

induced shift coefficients (in cm<sup>-1</sup>/atm at 294 K).  $b_{\rm L}(p, T)$  is the Lorentz half-width (in cm<sup>-1</sup>) of the spectral line at pressure *p* and temperature *T*.  $b_{\rm L}^{0}({\rm Gas})(p_0, T_0)$  is the Lorentz half-width coefficient of the line at the reference pressure  $p_0$  (1 atm) and temperature  $T_0$  (296 K) of the broadening gas (either Ar or CO<sub>2</sub> in the present case), and  $\chi$  is the ratio of the partial pressure of CO<sub>2</sub> to the total sample pressure in the cell.

The off diagonal relaxation matrix elements on one side of the diagonal are found from the coefficients provided. The other side is found from detailed balance for the two states with J and J + 2 for rotational quantum numbers,

$$W_{ji} = W_{ij} \frac{\rho(J+2) \times 2 \times (J+3)}{\rho(J) \times 2 \times (J+1)}$$

$$\tag{4}$$

Here  $\rho(J)$  is the population of molecules in the state with rotational quantum number J, as calculated from the Boltzman distribution and  $2 \times (J + 1)$  is the statistical weight of the same state. The relaxation matrix formulation for the calculation of line mixing is used for several reasons. The first is that it can be converted to the equivalent Rosenkranz formulation quite easily by the methods of refs. 33 and 34. but the inverse operation is either difficult (sometimes when the number of nonzero off-diagonal matrix elements determined is less than the number of lines mixing) or nonunique. Furthermore, the Rosenkranz formulation is only an approximation that breaks down at higher pressures where the separation of the lines is no longer much larger than the Lorentz width. The relaxation matrix elements also allow for the combination of mixing from simultaneous broadening by more than one gas. These elements also have physical meaning that allows them to be extended to other temperatures without measurement at every temperature. The Rosenkranz approximation can also lead to slightly different definitions of intensity, pressure shift, and zero-pressure position for different broadening gases, temperatures, and pressures.

The present analysis was performed for the P62–R58 transitions in the  $30012 \leftarrow 00001$  band, P62–R60 transitions in the  $30013 \leftarrow 00001$  band, and for P45–R46 in the  $31112 \leftarrow$ 01101 and  $31113 \leftarrow 01101$  bands. For weak transitions outside these ranges, Lorentz self-broadened half-width coefficients were held fixed to HITRAN values [35, 36]. The Arbroadened half-width coefficients for unmeasured transitions (transitions beyond our highest measured J") were fixed to our present values determined at the highest J" value. Both

Line	Position <sup>a</sup>	$b_L^0(\operatorname{Ar})^b$	Unc. (%)	$\delta^0(\operatorname{Ar})^c$ unc.	$SD^d$	Unc. (%)
P62e	6 165.898 26	0.052 90	5.12	-0.014 04 (264)	0.1	
P60e	6 168.353 90	0.049 10	3.63	-0.016 66 (173)	0.1	
P58e	6 170.777 30	0.046 18	2.19	-0.008 80 (99)	0.1	
P56e	6 173.168 65	0.047 46	1.50	-0.008 21 (69)	0.1	
P54e	6 175.528 18	0.047 87	1.04	-0.009 33 (49)	0.1	
P52e	6 177.856 09	0.049 05	0.75	-0.008 27 (35)	0.1	
P50e	6 180.152 60	0.049 54	0.61	-0.009 64 (29)	0.1	
P48e	6 182.417 93	0.050 27	0.40	-0.008 89 (19)	0.1	
P46e	6 184.652 30	0.050 04	0.48	-0.009 73 (23)	0.062	6.0
P44e	6 186.855 91	0.050 85	0.26	-0.008 50 (11)	0.098	2.2
P42e	6 189.029 00	0.051 58	0.21	-0.008 53 (9)	0.108	1.7
P40e	6 191.171 76	0.051 93	0.17	-0.008 92 (11)	0.087	2.3
P38e	6 193.284 40	0.052 00	0.15	-0.008 44 (9)	0.094	1.9
P36e	6 195.367 14	0.053 25	0.13	-0.008 34 (8)	0.108	1.5
P34e	6 197.420 14	0.053 40	0.11	-0.008 27 (7)	0.111	1.4
P32e	6 199.443 62	0.054 13	0.11	-0.008 11 (6)	0.109	1.4
P30e	6 201.437 74	0.054 76	0.13	-0.008 24 (7)	0.107	1.5
P28e	6 203.402 68	0.055 64	0.11	-0.008 05 (5)	0.113	1.3
P26e	6 205.338 59	0.056 12	0.11	-0.007 98 (5)	0.107	1.4
P24e	6 207.245 63	0.057 55	0.12	-0.007 48 (7)	0.131	1.1
P22e	6 209.123 93	0.058 66	0.10	-0.007 57 (5)	0.131	1.0
P20e	6 210.973 63	0.059 64	0.10	-0.007 16 (5)	0.131	1.0
P18e	6 212.794 85	0.061 17	0.10	-0.007 21 (5)	0.141	0.9
P16e	6 214.587 68	0.062 45	0.10	-0.007 09 (5)	0.126	1.1
P14e	6 216.352 21	0.064 47	0.11	-0.006 89 (6)	0.151	0.8
P12e	6 218.088 53	0.065 34	0.09	-0.006 35 (5)	0.146	0.8
P10e	6 219.796 71	0.067 20	0.12	-0.006 57 (7)	0.145	0.8
P08e	6 221.476 78	0.068 90	0.10	-0.005 74 (6)	0.136	0.9
P06e	6 223.128 78	0.070 34	0.10	-0.005 43 (7)	0.134	0.9
P04e	6 224.752 75	0.072 91	0.12	-0.005 53 (10)	0.127	1.0
P02e	6 226.348 68	0.077 05	0.18	-0.003 88 (17)	0.117	1.2
R00e	6 228.689 98	0.081 26	0.30	-0.001 60 (31)	0.091	2.6
R02e	6 230.215 76	0.074 09	0.13	-0.003 79 (11)	0.127	1.0
R04e	6 231.713 42	0.071 17	0.10	-0.004 18 (8)	0.118	1.1
R06e	6 233.182 89	0.069 13	0.10	-0.004 48 (6)	0.141	0.8
R08e	6 234.624 10	0.067 25	0.09	-0.004 42 (6)	0.139	0.9
R10e	6 236.036 97	0.065 35	0.09	-0.004 83 (5)	0.139	0.9
R12e	6 237.421 40	0.063 92	0.09	-0.005 30 (5)	0.136	0.9
R14e	6 238.777 27	0.062 17	0.10	-0.005 42 (5)	0.137	0.9
R16e	6 240.104 44	0.060 81	0.10	-0.005 85 (5)	0.130	1.0
R18e	6 241.402 78	0.059 65	0.10	-0.006 24 (5)	0.121	1.2
R20e	6 242.672 14	0.058 06	0.09	-0.006 25 (5)	0.113	1.3
R22e	6 243.912 34	0.057 22	0.10	-0.006 70 (5)	0.124	1.1
R24e	6 245.123 21	0.056 04	0.11	-0.006 73 (5)	0.105	1.5
R26e	6 246.304 55	0.055 25	0.10	-0.007 09 (5)	0.105	1.6
R28e	6 247.456 16	0.054 26	0.11	-0.007 44 (5)	0.094	1.8
R30e	6 248.577 83	0.053 70	0.11	-0.007 46 (6)	0.100	1.7
R32e	6 249.669 34	0.053 20	0.11	-0.007 47 (6)	0.091	2.0
R34e	6 250.730 46	0.052 43	0.11	-0.007 94 (7)	0.072	2.9
R36e	6 251.760 95	0.052 21	0.13	-0.007 93 (8)	0.098	1.8
R38e	6 252.760 57	0.051 52	0.16	-0.008 19 (9)	0.075	2.9
R40e	6 253.729 06	0.050 68	0.18	-0.008 24 (7)	0.077	2.8
R42e	6 254.666 16	0.050 63	0.20	-0.008 51 (9)	0.083	2.6
R44e	6 255.571 62	0.050 23	0.24	-0.009 01 (11)	0.096	2.3
R46e	6 256.445 16	0.049 61	0.30	-0.009 83 (14)	0.103	2.4
R48e	6 257.286 53	0.049 29	0.39	-0.009 30 (18)	0.1	

**Table 3.** Ar-broadened half-width and pressure-induced shift coefficients and speed dependence in the  $30013 \leftarrow 00001$  band of  ${}^{16}O^{12}C^{16}O$ .

$b_L^0(\operatorname{Ar})^b$	Unc. (%)	$\delta^0(\operatorname{Ar})^c$ unc.	$SD^d$	Unc. (%)
0.048 16	0.52	-0.008 37 (24)	0.1	
0.047 65	0.71	-0.010 03 (33)	0.1	
0.047 24	1.01	-0.008 80 (46)	0.1	

-0.009 10 (69)

-0.009 85 (94)

-0.009 99 (150)

Table 3 (concluded).

Position<sup>a</sup>

6 258.095 45

6 258.871 66

6 259.614 88

6 260.324 86

6 261.001 32

6 261.644 02

Line

R50e

R52e

R54e

R56e

R58e

R60e

"Zero-pressure line center positions are in cm<sup>-1</sup>. While the position values were adjusted during the present study,

1.44

2.11

3.18

to the accuracy given here they are the same as in [5]. See text for details.

0.047 80

0.045 10

0.047 55

<sup>b</sup>The measured Ar-broadened half-width coefficients are in cm<sup>-1</sup>/atm at 296 K.

<sup>c</sup>The measured Ar-induced pressure-shift coefficients are in cm<sup>-1</sup>/atm at the temperature of the spectra ( $\sim 294$  K;

see Table 1).

<sup>d</sup>Speed-dependence (SD) parameter (unitless).

self- and Ar-induced pressure-shift coefficients for unfitted transitions were fixed to a default value of -0.005 cm<sup>-1</sup>/ atm, a value that is comparable to the majority of the measured pressure-induced shift coefficients in this wavenumber region [4, 5]. The temperature dependence exponents of the Ar-broadened half-width  $(n_1 \text{ in } (1))$  and the self-broadened half-width coefficient  $(n_2 \text{ in } (1))$  were assumed equal to the  $n_1$  values in HITRAN [35, 36], which range between 0.69 and 0.78 depending upon the J'' value of the transition. Since the gas temperatures in the present data were close to 296 K, assuming identical temperature exponents for both and self- and Ar-broadening introduced errors no larger than 0.05% in the retrieved broadening coefficients. The temperature dependences of all self- and Ar-shift coefficients were set to zero. This assumption also introduced no noticeable residuals in the least-squares fits.

# 4. Results and discussion

## 4.1. Ar-broadened half-width and pressure-shift coefficients

The final multispectrum fit to all 21 spectra for the 6280 to 6395 cm<sup>-1</sup> interval covering 30012←00001 band is plotted in Fig. 1. Weaker absorption features from the  $31112 \leftarrow$ 01101 hot band and other interfering hot band and isotopologue lines also appear in the fitted region. Figure 1a shows the 21 observed spectra. Figure 1b shows the weighted fit residuals from all 21 spectra using a speed-dependent Voigt profile and line mixing calculated via the relaxation matrix [33, 34]. Figure 1c shows only the weighted fit residuals from the 6 Ar-broadened spectra (copied from Fig. 1b for purpose of illustration). Panels b and c of Fig. 1 demonstrate that the signal-to-noise based weighting scheme produces consistently high quality fits in all spectra.

The results from the multispectrum least-squares fits are listed in Tables 2–6. The results for the 30012←00001 band are given in Table 2. The rovibrational (G, B, D, H, ...) and intensity  $(S_{\nu}, a_1, a_2)$  parameters were constrained to the values reported in [4]. The self-broadened half-width and selfshift coefficients, as well as the self induced off-diagonal relaxation matrix elements were also fixed to the measured values from [4]. This procedure ensures maximum accuracy in the Ar-broadened half-width and pressure shift coefficients as well as consistency with our previous work. To confirm the robustness of the Ar-broadened multispectrum fit, the rovibrational (G, B, D, H,...) and intensity ( $S_v$ ,  $a_1$ ,  $a_2$ ) parameters were floated in the final fit to determine how much variation this introduced into the results. As expected, the final parameter values determined in the present study were well within the uncertainty ranges for all of the parameters reported in [4]. The truncated positions listed in Table 2 are presented for ease in identifying different transitions

0.1

0.1

0.1

The Lorentz Ar pressure-broadened half-width coefficients  $b_L^0$  (Ar) (in cm<sup>-1</sup>/atm at 296 K), the Ar pressure-induced shift coefficients  $\delta^0(Ar)$  (in cm<sup>-1</sup>/atm at ~294 K), and the values determined from the least-squares fit for speed dependence parameters (unitless) for self- and Arbroadening are also listed in Table 2. Since no temperature dependence was assumed for the Ar pressure-induced shift coefficients  $\delta^{0}(Ar)$ , the listed values correspond to the temperature of the data ( $\sim 294$  K). For the Ar pressure-broadened half-width coefficients  $b_L^0$  (Ar), a default value of 0.75 was used as the temperature dependence exponent for all transitions, and hence the values listed correspond to a reference temperature of 296 K, as assumed in HITRAN database [35, 36]. The uncertainties in Ar-broadened half-width coefficients and speed dependence parameters are given as percentages. The measured uncertainties in the Ar pressureshift coefficients listed in parentheses are in units of the least significant digits reported. The uncertainty represents one standard deviation in the measured quantity in all instances.

Table 3 presents the results for the  $30013 \leftarrow 00001$  band. As with the  $30012 \leftarrow 00001$  multispectrum fit, the line positions, intensities, self-broadened half-widths, and self-induced shift coefficients for bands studied in [5] were held fixed during the analysis of Ar-broadened half-width and pressure-shift coefficients for the  $30013 \leftarrow 00001$  band. The test fit floated the rovibrational (G, B, D, H, ...) and intensity  $(S_{v}, a_{1}, a_{2})$  parameters and these were determined within the experimental uncertainties reported in [5].

Ar-broadened half-width and Ar-induced pressure-shift coefficients for the  $31112 \leftarrow 01101$  and the  $31113 \leftarrow 01101$ hot bands were also measured because of the fairly large volume mixing ratios of CO<sub>2</sub> in the Ar-broadened spectra used in this work and compared with the air-broadened spectra analyzed in the previous investigations [4, 5]. The measurements obtained for the hot band transitions are less extensive and less accurate than the values obtained for the

**Table 4.** Ar-broadened half-width and pressure-shift coefficients in the  $31112 \leftarrow 01101$  band of  ${}^{16}O{}^{12}C{}^{16}O$ .

Table 4 (concluded).

			Unc.	
Line	Position <sup>a</sup>	$b_L^0(\operatorname{Ar})^b$	(%)	$\delta^0(\mathbf{Ar})^c$ unc.
P45e	6 313.548 92	0.041 90	6.99	
P43e	6 315.771 07	0.047 34	5.39	-0.006 35 (256)
P41e	6 317.964 14	0.049 90	4.17	-0.004 75 (208)
P39e	6 320.127 97	0.054 59	4.07	-0.012 13 (222)
P37e	6 322.262 38	0.048 72	3.63	-0.009 55 (178)
P35e	6 324.367 23	0.059 25	2.16	-0.007 36 (128)
P33e	6 326.442 36	0.053 08	1.70	-0.013 15 (90)
P31e	6 328.487 64	0.052 28	1.43	-0.008 67 (75)
P29e	6 330.502 94	0.053 99	1.28	-0.009 36 (68)
P27e	6 332.488 13	0.056 93	1.32	-0.008 89 (74)
P25e	6 334.443 10	0.044 73	4.29	-0.014 62 (187)
P23e	6 336.367 75	0.056 75	1.21	-0.005 30 (70)
P21e	6 338.261 97	0.059 30	0.86	-0.006 80 (51)
P19e	6 340.125 66	0.060 24	0.78	-0.007 26 (46)
P17e	6 341.958 75	0.062 81	0.75	-0.005 88 (47)
P15e	6 343.761 15	0.061 94	0.74	-0.005 12 (46)
P13e	6 345.532 79	0.062 50	0.77	-0.006 68 (47)
P11e	6 347.273 61	0.064 38	0.82	-0.005 38 (53)
P09e	6 348.983 53	0.068 36	0.95	-0.005 98 (65)
P05e	6 352.310 49	0.068 15	1.58	-0.004 10 (107)
P03e	6 353.927 44	0.078 31	2.83	-0.011 28 (222)
R01e	6 357.833 81	0.066 11	4.87	-0.005 16 (322)
R03e	6 359.341 89	0.071 83	2.02	-0.004 90 (144)
R05e	6 360.818 82	0.071 72	1.37	-0.004 42 (98)
R0/e	6 362.264 59	0.070 86	1.16	-0.006 37 (82)
R09e	6 363.679 19	0.067 47	2.43	-0.001 03 (163)
RIIe	6 365.062 62	0.066 45	1.02	-0.005 97 (68)
RI3e	6 366.414 91	0.063 44	0.76	-0.004 20 (47)
RI5e	6 367.736 06	0.060 43	0.71	-0.006 12 (43)
RI/e	6 369.026 09	0.059 26	0.73	-0.004 95 (42)
R19e	6 370.285 03	0.059 45	0.81	-0.006 40 (47)
R21e	6 3/1.512 91	0.055 /3	1.81	-0.007 81 (103)
K25e	6 372.709 79	0.055 49	0.88	-0.007 13 (48)
K25e	0 3/3.8/3 /0	0.057 32	1.24	-0.006 54 (70)
R2/e	0 3/3.010 /0	0.051 22	1.02	-0.005 11 (85)
R29e	6 277 199 25	0.052 18	1.07	-0.00790(87)
D22a	6 278 220 04	0.052.57	1.41	-0.00044(74)
R350 R350	6 370 243 01	0.052 02	2.02	-0.00977(87)
R330 D370	6 380 224 58	0.051 10	2.02	-0.00973(103)
R370 D30a	6 381 175 73	0.052 78	3 21	$-0.003\ 00\ (231)$
R390	6 383 847 88	0.041 78	7.10	-0.007 23 (103) 0.015 03 (207)
P46f	6 313 948 49	0.050.48	7.10 8.60	-0.015 05 (297)
$P_{1/1f}$	6 316 050 49	0.043 50	6.15	0.011.68 (260)
P42f	6 318 129 89	0.051.59	4.87	$-0.011\ 00\ (20)$
P40f	6 320 186 50	0.050.83	4 58	-0.008.97(233)
P38f	6 322 220 11	0.054 32	4 20	-0.01357(228)
P36f	6 324 230 54	0.053.06	2.36	-0.005 88 (125)
P34f	6 326 217 60	0.054 79	1.88	-0.00772(103)
P32f	6 328.181 14	0.054 24	1.55	-0.004 57 (83)
P30f	6 330.120 98	0.057 01	1.33	-0.007 55 (75)
P28f	6 332.037 00	0.053 99	1.13	-0.008 78 (61)
P26f	6 333.929 03	0.057 35	1.01	-0.008 69 (58)
P24f	6 335.796 95	0.056 53	0.92	-0.007 33 (52)
P22f	6 337.640 64	0.058 14	0.86	-0.008 14 (50)
P20f	6 339.459 98	0.060 77	0.86	-0.008 85 (52)
-			-	(- =)

			Unc.	
Line	Position <sup>a</sup>	$b_L^0(\mathrm{Ar})^b$	(%)	$\delta^0(Ar)^c$ unc.
P18f	6 341.254 86	0.060 43	0.96	-0.007 10 (59)
P16f	6 343.025 19	0.058 26	2.47	-0.002 88 (136)
P14f	6 344.770 87	0.064 22	1.09	-0.007 75 (75)
P12f	6 346.491 82	0.064 24	0.84	-0.007 74 (53)
P10f	6 348.187 97	0.067 18	0.88	-0.006 99 (59)
P08f	6 349.859 25	0.071 30	1.08	-0.007 00 (76)
P06f	6 351.505 60	0.074 89	1.71	-0.001 62 (132)
P04f	6 353.126 97	0.067 64	7.92	0.000 42 (509)
P02f	6 354.723 31	0.072 73	6.00	-0.007 77 (436)
R02f	6 358.604 48	0.065 30	7.61	-0.009 40 (498)
R04f	6 360.113 01	0.073 02	2.15	0.001 01 (159)
R06f	6 361.596 42	0.068 32	1.20	-0.002 13 (82)
R08f	6 363.054 70	0.066 50	0.95	-0.004 54 (63)
R10f	6 364.487 87	0.064 49	0.84	-0.003 44 (53)
R12f	6 365.895 93	0.063 65	0.86	-0.005 03 (54)
R14f	6 367.278 91	0.064 39	1.44	-0.004 83 (97)
R16f	6 368.636 84	0.062 16	0.74	-0.004 51 (45)
R18f	6 369.969 75	0.060 41	0.73	-0.007 25 (43)
R20f	6 371.277 70	0.058 54	0.80	-0.004 55 (46)
R22f	6 372.560 74	0.056 41	1.03	-0.005 63 (60)
R24f	6 373.818 93	0.053 27	1.16	-0.004 87 (61)
R26f	6 375.052 34	0.056 78	1.57	-0.007 65 (88)
R28f	6 376.261 06	0.053 81	1.28	-0.009 11 (68)
R30f	6 377.445 17	0.050 71	1.26	-0.010 38 (64)
R32f	6 378.604 77	0.056 47	2.00	-0.008 60 (112)
R34f	6 379.739 96	0.055 31	1.86	-0.009 11 (102)
R36f	6 380.850 87	0.058 10	2.65	-0.008 87 (154)
R38f	6 381.937 61	0.049 03	2.86	-0.009 82 (140)
R42f	6 384.039 16	0.048 86	4.72	-0.010 88 (232)
R44f	6 385.054 27	0.037 73	6.07	-0.017 06 (230)
R46f	6 386.045 81	0.043 13	8.37	

<sup>*a*</sup>Zero pressure line center positions are in  $cm^{-1}$ . The position values are the same as in [4] and were held fixed during the present study.

 $^{b}$ The measured Ar-broadened half-width coefficients are in cm<sup>-1</sup>/atm at 296 K.

<sup>c</sup>The measured Ar-induced pressure-shift coefficients are in cm<sup>-1</sup>/atm at the temperature of the spectra ( $\sim 294$  K; see Table 1).

stronger  $30012 \leftarrow 00001$  and the  $30013 \leftarrow 00001$  bands. The results obtained for the  $31112 \leftarrow 01101$  and the  $31113 \leftarrow 01101$  bands are listed in Tables 4 and 5, respectively. Because the transitions in these hot bands were weak, line mixing and speed dependence were neither determinable nor required to fit the data for these bands to the experimental noise level (see Fig. 1).

The measured Ar-broadened half-width coefficients for the  $30012 \leftarrow 00001$  and the  $30013 \leftarrow 00001$  bands and the associated  $31112 \leftarrow 01101$  and  $31113 \leftarrow 01101$  hot bands are plotted as a function of m (m = -J'' and J'' + 1, for the Pand R-branch transitions) in Fig. 2. The Q-branch transitions in the  $31112 \leftarrow 01101$  and the  $31113 \leftarrow 01101$  were weak, and neither broadening nor shift coefficients were measured for those transitions. The parameters for  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands are plotted in panel (Fig. 2*a*), and the corresponding values for the  $31112 \leftarrow 01101$  and the  $31113 \leftarrow 01101$  bands in panel (Fig. 2*b*). The Ar-broadened half-width coefficients of Valero and Suarez [11], Suarez

**Table 5.** Ar-broadened half-width and pressure-induced shift coefficients in the  $31113 \leftarrow 01101$  band of  ${}^{16}O^{12}C^{16}O$ .

		0 I	Unc.	<u>.</u>
Line	Position <sup>a</sup>	$b_L^0(\operatorname{Ar})^b$	(%)	$\delta^0(\mathrm{Ar})^c$
P45e	6 153.693 42	0.047 15	6.26	-0.012 30 (296)
P43e	6 155.900 06	0.051 17	4.81	-0.003 40 (247)
P41e	6 158.076 76	0.053 09	3.72	-0.013 21 (199)
P39e	6 160.223 62	0.049 75	3.05	-0.008 93 (152)
P35e	6 164.428 19	0.057 19	2.03	-0.008 00 (116)
P33e	6 166.486 03	0.054 21	1.53	-0.007 89 (83)
P31e	6 168.514 30	0.056 34	1.31	-0.007 20 (74)
P29e	6 170.513 04	0.054 60	1.09	-0.008 48 (60)
P27e	6 172.482 27	0.056 20	0.96	-0.007 21 (54)
P25e	6 174.421 99	0.056 99	0.86	-0.007 99 (49)
P23e	6 176.332 22	0.057 89	0.80	-0.007 34 (45)
P21e	6 178.212 96	0.058 31	0.74	-0.006 36 (42)
P19e	6 180.064 19	0.058 24	0.79	-0.007 10 (46)
P17e	6 181.885 90	0.059 86	0.68	-0.006 68 (41)
P15e	6 183.678 09	0.062 73	0.70	-0.006 95 (43)
P13e	6 185.440 72	0.064 50	0.73	-0.006 15 (46)
P11e	6 187.173 79	0.066 76	0.79	-0.005 23 (52)
P09e	6 188.877 26	0.070 41	0.95	-0.005 78 (67)
P07e	6 190.551 11	0.069 97	1.09	-0.005 74 (76)
P05e	6 192.195 32	0.070 79	1.48	-0.008 67 (104)
R05e	6 200.707 42	0.069 63	1.22	-0.006 69 (85)
R07e	6 202.158 32	0.068 23	0.95	-0.004 24 (64)
R09e	6 203.579 37	0.068 99	0.93	-0.004 39 (63)
R11e	6 204.970 55	0.064 40	0.75	-0.003 24 (47)
R13e	6 206.331 84	0.063 30	0.68	-0.006 10 (42)
R15e	6 207.663 21	0.061 67	0.66	-0.004 52 (41)
R17e	6 208.964 61	0.061 55	0.81	-0.005 11 (50)
R19e	6 210.236 02	0.058 89	0.68	-0.007 08 (39)
R21e	6 211.477 39	0.057 94	0.72	-0.006 81 (41)
R23e	6 212.688 68	0.054 46	1.23	-0.007 41 (68)
R25e	6 213.869 84	0.055 54	1.29	-0.008 18 (72)
R27e	6 215.020 81	0.055 22	1.26	-0.005 99 (70)
R29e	6 216.141 53	0.056 45	1.28	-0.006 63 (72)
R31e	6 217.231 92	0.053 60	1.25	-0.005 93 (67)
R33e	6 218.291 90	0.054 80	1.73	-0.009 97 (94)
R35e	6 219.321 38	0.053 90	1.81	-0.006 40 (98)
R37e	6 220.320 23	0.052 30	2.22	-0.006 80 (116)
R41e	6 222.225 57	0.050 62	3.56	-0.006 66 (181)
R45e	6 224.006 72	0.053 37	6.26	
R47e	6 224.850 25	0.053 05	11.12	
P48f	6 152.010 23	0.042 35	9.66	-0.010 57 (410)
P46f	6 154.124 41	0.043 53	7.28	-0.005 54 (318)
P44f	6 156.213 97	0.049 59	5.51	-0.007 41 (274)
P42f	6 158.279 10	0.041 96	4.22	-0.011 33 (177)
P40f	6 160.319 94	0.046 94	3.43	-0.012 79 (161)
P36f	6 164.329 38	0.049 68	2.19	-0.004 47 (109)
P34f	6 166.298 22	0.054 64	1.70	-0.005 81 (93)
P32f	6 168.243 28	0.053 31	1.48	-0.005 84 (79)
P30f	6 170.164 66	0.055 94	1.19	-0.008 16 (67)
P28f	6 172.062 43	0.055 16	1.03	-0.006 22 (56)
P26f	6 173.936 66	0.053 67	0.91	-0.004 57 (48)
P24f	6 175.787 41	0.057 27	0.82	-0.006 07 (47)
P22f	6 177.614 74	0.057 00	0.75	-0.007 34 (43)
P20f	6 179.418 68	0.059 56	0.72	-0.007 74 (42)
P18f	6 181.199 27	0.061 35	0.70	-0.006 29 (42)
P16f	6 182.956 53	0.061 69	0.70	-0.006 98 (42)

Table 5 (concluded).

			Unc.	
Line	Position <sup>a</sup>	$b_L^0(\operatorname{Ar})^b$	(%)	$\delta^0(\mathrm{Ar})^c$
P14f	6 184.690 49	0.060 01	1.15	-0.005 12 (67)
P12f	6 186.401 16	0.063 27	0.74	-0.004 49 (47)
P10f	6 188.088 53	0.066 39	0.83	-0.005 93 (55)
P08f	6 189.752 63	0.068 05	0.97	-0.008 18 (66)
P06f	6 191.393 43	0.071 82	1.31	-0.011 34 (92)
P04f	6 193.010 93	0.074 15	1.93	-0.008 15 (141)
R04f	6 200.000 85	0.070 16	1.45	-0.005 68 (102)
R06f	6 201.489 80	0.066 56	2.05	-0.004 79 (145)
R08f	6 202.955 27	0.067 23	0.88	-0.005 60 (58)
R10f	6 204.397 21	0.064 62	0.76	-0.003 60 (48)
R12f	6 205.815 55	0.062 30	0.70	-0.005 55 (43)
R16f	6 208.581 25	0.061 54	0.67	-0.006 58 (40)
R18f	6 209.928 45	0.058 77	0.66	-0.005 63 (38)
R20f	6 211.251 80	0.058 33	0.73	-0.004 68 (43)
R22f	6 212.551 20	0.057 57	0.83	-0.006 47 (48)
R24f	6 213.826 56	0.056 73	1.26	-0.005 98 (71)
R26f	6 215.077 77	0.055 77	1.18	-0.007 41 (66)
R28f	6 216.304 73	0.048 93	2.84	-0.004 95 (135)
R30f	6 217.507 31	0.054 09	1.16	-0.007 79 (62)
R32f	6 218.685 39	0.052 62	1.37	-0.006 49 (71)
R34f	6 219.838 81	0.050 56	4.41	-0.001 71 (217)
R36f	6 220.967 42	0.054 48	2.02	-0.009 37 (110)
R38f	6 222.071 06	0.049 66	2.50	-0.011 52 (124)
R42f	6 224.202 65	0.054 12	4.10	-0.007 14 (222)
R44f	6 225.230 19	0.053 17	5.44	-0.011 03 (291)
R46f	6 226.231 93	0.048 84	8.39	

 ${}^{a}$ Zero-pressure line center positions are in cm<sup>-1</sup>. The position values are the same as in [5] and were held fixed during the present study.

 ${}^{b}$ The measured Ar-broadened half-width coefficients are in cm<sup>-1</sup>/atm at 296 K.

<sup>c</sup>The measured Ar-induced pressure-shift coefficients are in cm<sup>-1</sup>/atm at the temperature of the spectra ( $\sim 294$  K; see Table 1).

and Valero [12], Nakamichi et al. [30], Thibault et al. [13], and Li et al. [32] are also plotted in Fig. 2a for comparison. The agreement between our results and those of Valero and Suarez [11] is good, especially for transitions with  $10 \le m \le$ 30, despite the significant differences in uncertainties, instrumentation, resolution, data analysis methods, etc. The results reported by Nakamichi et al. [30] for transitions in the 30013←00001 compare well with present measurements, except for R0. Although there is good agreement in the Rbranch measurements between present study and the measurements of  $3v_3$  band by Thibault et al. [13], there are some differences seen in the results for the P-branch transitions. The values of Li et al. [32] for R0 to R20 average slightly higher than the present results. As can be expected, the uncertainties in the Ar-broadened half-width coefficients for the  $31112 \leftarrow 01101$  and the  $31113 \leftarrow 01101$  bands (Fig. 2b) are larger than those for the 30012←00001 and the 30012←00001 bands.

The measured Ar-broadened half-width coefficients for lines in the  $30012 \leftarrow 00001$  and the  $30013 \leftarrow 00001$  bands are compared with previously measured self- and air-broadening coefficients [4, 5] and the half-width coefficients for all three broadening gases are plotted as a function of *m* in Fig. 3. The results for the  $30012 \leftarrow 00001$  band are plotted

**Table 6.** Off-diagonal relaxation matrix element coefficients ( $W_{ij}$ ) for 30012  $\leftarrow$  00001 and 30013–00001 bands of <sup>16</sup>O <sup>12</sup>C<sup>16</sup>O for CO<sub>2</sub>–Ar broadening.

	Self- $W_{ii}^{CO_2-CO_2}(296 \text{ K})$	Air- $W_{ii}^{CO_2-air}(296 \text{ K})$	Argon- $W_{::}^{CO_2-Ar}(296 \text{ K})$	Argon- $W_{::}^{CO_2-Ar}(296 \text{ K})$
Line mixing between	30012←00001	30012←00001	30012←00001	30013←00001
P2 to P4	0.0076 (1)	0.0087 (8)	0.0047(6)	0.0034(6)
P4 to P6	0.0137 (1)	0.0117 (8)	0.0035(6)	0.0078(6)
P6 to P8	0.0175 (2)	0.0163 (8)	0.0072(6)	0.0101(6)
P8 to P10	0.0207 (2)	0.0186 (8)	0.0113(6)	0.0135(6)
P10 to P12	0.0227 (2)	0.0205 (8)	0.0129(6)	0.0136(6)
P12 to P14	0.0248 (2)	0.0214 (8)	0.0145(6)	0.0168(6)
P14 to P16	0.0266 (2)	0.0241 (9)	0.0160(7)	0.0180(7)
P16 to P18	0.0274 (2)	0.0228 (9)	0.0167(7)	0.0190(7)
P18 to P20	0.0283 (2)	0.0241 (10)	0.0184(7)	0.0183(7)
P20 to P22	0.0282 (2)	0.0271 (10)	0.0178(8)	0.0186(8)
P22 to P24	0.0285 (2)	0.0253 (11)	0.0176(8)	0.0179(8)
P24 to P26	0.0279 (2)	0.0241 (12)	0.0169(9)	0.0179(9)
P26 to P28	0.0267 (3)	0.0219 (14)	0.0163(10)	0.0156(10)
P28 to P30	0.0256 (3)	0.0204 (15)	0.0170(11)	0.0141(11)
P30 to P32	0.0238 (3)	0.0159 (16)	0.0141(12)	0.0112(12)
P32 to P34	0.0213 (3)	0.0120 (17)	0.0137(12)	0.0103(13)
P34 to P36	0.0163 (3)	0.0087 (18)	0.0112(12)	0.0104(14)
P36 to P38	0.0131 (3)	0.0088 (16)	0.0125(11)	0.0089(15)
P38 to P40	0.0099 (3)	0.004 Fixed	0.004 Fixed	0.0087(13)
P40 to P42	0.0064 (3)	0.004 Fixed	0.004 Fixed	0.004 Fixed
P42 to P44	0.004 Fixed	0.004 Fixed	0.004 Fixed	0.004 Fixed
P44 to P46	0.004 Fixed	0.004 Fixed	0.004 Fixed	0.004 Fixed
P46 to P48	0.004 Fixed	0.004 Fixed	0.004 Fixed	0.004 Fixed
P48 to P50	0.004 Fixed	0.004 Fixed	0.004 Fixed	0.004 Fixed
R0 to R2	0.0048 (1)	0.0034 (6)	0.0012(4)	0.0007(4)
R2 to R4	0.0156 (1)	0.0112 (8)	0.0080(6)	0.0072(6)
R4 to R6	0.0215 (1)	0.0155 (8)	0.0117(6)	0.0093(6)
R6 to R8	0.0256 (2)	0.0201 (7)	0.0139(6)	0.0121(5)
R8 to R10	0.0288 (2)	0.0212 (7)	0.0148(5)	0.0127(5)
R10 to R12	0.0306 (2)	0.0213 (6)	0.0145(5)	0.0135(5)
R12 to R14	0.0320 (2)	0.0216 (6)	0.0149(5)	0.0145(5)
R14 to R16	0.0333 (2)	0.0223 (7)	0.0153(5)	0.0146(5)
R16 to R18	0.0338 (2)	0.0234 (7)	0.0159(5)	0.0148(5)
R18 to R20	0.0335 (2)	0.0233 (7)	0.0163(5)	0.0149(5)
R20 to R22	0.0328 (2)	0.0237 (7)	0.0156(6)	0.0147(5)
R22 to R24	0.0319 (2)	0.0232 (7)	0.0153(6)	0.0151(5)
R24 to R26	0.0310 (2)	0.0222 (8)	0.0147(6)	0.0142(5)
R26 to R28	0.0296 (2)	0.0222 (8)	0.0140(7)	0.0135(5)
R28 to R30	0.0288 (2)	0.0206 (9)	0.0135(7)	0.0138(5)
R30 to R32	0.0272 (3)	0.0191 (10)	0.0109(8)	0.0139(6)
R32 to R34	0.0257 (3)	0.0175 (10)	0.0113(8)	0.0115(6)
R34 to R36	0.0239 (3)	0.0165 (11)	0.0116(8)	0.0108(5)
R36 to R38	0.0211 (3)	0.0106 (11)	0.0098(7)	0.0096(5)
R38 to R40	0.0184 (3)	0.0078 (10)	0.0057(7)	0.004 Fixed
R40 to R42	0.0164 (4)	0.004 Fixed	0.004 Fixed	0.004 Fixed
R42 to R44	0.0130 (4)	0.004 Fixed	0.004 Fixed	0.004 Fixed
R44 to R46	0.0095 (4)	0.004 Fixed	0.004 Fixed	0.004 Fixed
R46 to R48	0.0070 (4)	0.004 Fixed	0.004 Fixed	0.004 Fixed
R48 to R50	0.0050 (4)	0.004 Fixed	0.004 Fixed	0.004 Fixed

**Note:** Units are cm<sup>-1</sup>/atm near 296 K. The values given in parentheses represent one standard deviation uncertainties in the last quoted digits. The offdiagonal relaxation matrix element coefficients for self- and air-broadening (as examples) are listed only for the  $30012 \leftarrow 00001$  band. The corresponding values for the  $30013 \leftarrow 00001$  are available in ref. 5.

on the left-side panels and those for the  $30013 \leftarrow 00001$  band on the right-side panels. Similar to previous studies [4, 5] the Ar-broadened half-width coefficients are fitted to the empirical functions given in Toth et al. [2, 3]. It is clear that for a given transition the Ar-broadened half-width coefficient (circles) is smaller than both the self- and air-

**Fig. 2.** Comparison of measured Ar-broadened half-width coefficients in  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$ ; and in  $31112 \leftarrow 01101$  and  $31113 \leftarrow 01101$  bands using the same spectra and analysis technique. (*a*) Measured Ar-broadened half-width coefficients (cm<sup>-1</sup>/atm at 296 K) of the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands of  ${}^{16}O^{12}C^{16}O$  plotted as a function of m (m = -J'' for P-branch lines and J'' + 1 for R-branch lines). CO<sub>2</sub>-Ar half-width coefficients measured by several investigators for the same bands as in present study and also by Thibault et al. [13] for the  $3v_3$  band are plotted for comparison. (*b*) Measured Ar-broadened half-width coefficients (cm<sup>-1</sup>/atm at 296 K) of the  $31112 \leftarrow 01101$  and  $31113 \leftarrow 01101$  bands of  ${}^{16}O^{12}C^{16}O$  plotted as a function of *m*. For clarity, transitions for the *e* and *f* species are plotted separately. Where error bars are not visible, the measured uncertainties are smaller than the size of the symbols used.



broadened half-width coefficients. The three curves (dashed, dash-dot-dash, and solid) passing through the corresponding measured points (Fig. 3, panels 3*a* and 3*d*) represent calculated self-, air- and Ar-broadened half-width coefficients, respectively.

The percentage differences between the measured and empirically calculated Ar-broadened half-width coefficients for the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands are plotted as a function of *m* in Figs. 3*b* and 3*e*, respectively. The differences in both cases are within  $\pm 1.5\%$ , except for a few high-*J* transitions where the weak absorptions are fitted with lower accuracy. The measured line-to-line variation is smooth to the 0.1% level, as seen in Figs. 3*a* and 3d and in values given in Tables 2 and 3. Since the measured halfwidth coefficients are not completely represented by the systematically different calculated values from the fitted curves, the parameters of the fit are not given and the measured values should be used instead. Closer examination of the residuals plotted in Figs. 3b and 3e indicates small systematic *m*dependent differences. These residuals exceed the typical line-to-line variations seen in Figs. 3a and 3d and are similar in magnitude to the percentage differences previously observed for self- and air-broadened half-width coefficients (see Fig. 8 of [4] and Fig. 7 of [5]). However, the systematic differences in the percentage residuals between the P- and R-branch lines suggest that the measured half-width coefficients for P- and R-branch transitions differ for the same |m|. The mean and standard deviation of the ratios of P- to **Fig. 3.** Comparison of measured self-, air-, and Ar-broadened half-width coefficients in  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands using the same spectra and analysis technique. The results for the  $30012 \leftarrow 00001$  band are plotted on the left side panels (*a*)–(*c*) and those for the  $30013 \leftarrow 00001$  bands on the right side panels (*d*)–(*f*). (*a*) Measured Ar-broadened half-width coefficients (cm<sup>-1</sup>/atm at 296 K) of the  $30012 \leftarrow 00001$  band of  ${}^{16}O^{12}C^{16}O$  are re-plotted as a function of *m*. The measured Ar-broadened half-width coefficients are fitted to the empirical expression given in [2, 3], and the calculated half-width coefficients are plotted by a solid curve. The self- and air-broadened half-width coefficients from our previous study [4] are also plotted for comparison purposes. (*b*) The percentage observed minus calculated residuals obtained for Ar-broadened half-width coefficients are plotted as a function of *m*. The ratios of self- to air and air- to Ar-broadened half-width coefficients are also plotted for comparison. Similar results for the  $30013 \leftarrow 00001$  band are displayed in (*d*)–(*f*). Where error bars are not visible the uncertainties are smaller than the size of the symbols used.



R-branch Ar-broadened half-width coefficients in both bands are calculated to be  $\sim 1.02 \pm 0.01$ . These small differences are responsible for the positive and negative percentage differences seen in Figs. 3b and 3e. There are hints of this Pbranch–R-branch asymmetry in the self- and air-broadened half-width coefficients reported in refs. 4, 5, but the pattern is not as pronounced as it is for Ar-broadened half-width coefficients. The calculated half-width coefficients do not represent the measured data to its fullest accuracy, so the best values to use are the measured values.

The ratios of self- to air-, self- to Ar-, and air- to Arbroadened half-width coefficients determined for  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands as a function of *m* are plotted in Figs. 3*c* and 3*f*, respectively. These ratios vary with

**Fig. 4.** Comparison of Ar-shift coefficients. (*a*) Measured Ar pressure-shift coefficients for the  $30012 \leftarrow 00001$  and the  $30013 \leftarrow 00001$  bands of  ${}^{16}O{}^{12}C{}^{16}O$  (cm<sup>-1</sup>/atm at ~294 K) are plotted as a function of m. CO<sub>2</sub>–Ar pressure-shift coefficients from Thibault et al. [13] for the  $3v_3$  band are plotted for comparison. (*b*) Measured Ar pressure-shift coefficients for the  $31112 \leftarrow 01101$  and  $31113 \leftarrow 01101$  bands of  ${}^{16}O{}^{12}C{}^{16}O$  (cm<sup>-1</sup>/atm at ~294 K) are plotted as a function of *m*. Where error bars are not visible, the uncertainties are smaller than the size of the symbols used.



m, as also seen in Figs. 3a and 3d. The mean and standard deviations of these ratios (self- to air-broadening, self- to-Ar broadening, and air- to Ar-broadening) for the 30012← 00001 band are found to be 1.26 and 0.09, 1.61 and 0.06, and 1.28 and 0.06, respectively. The ratios of the self- to Ar-broadened half-width coefficients have maxima near P28 and R28. The ratio increases from  $\sim 1.6$  near the center of the band to  $\sim 1.7$  near the maxima and then slowly falls off to  $\sim 1.55$  toward higher-J transitions. Beyond the P48 and R48 lines, the ratios tend to increase slowly. The general patterns in the variations of self- to air- and self- to Arbroadening with m are similar, although there is a shift in the self- to Ar-broadened half-width coefficients (higher) relative to those of self- to air-broadening. The pattern observed for the variations of air- to Ar-broadening with m is quite different from the other two cases; the ratio has a minimum of ~1.2 near the center of the band and gradually increases to 1.4 with higher *m* in both branches. Very similar values are obtained for the  $30013 \leftarrow 00001$  band. Corresponding plots for the  $30013 \leftarrow 00001$  band are displayed on the right-side panels of Fig. 3. Where error bars are not visible, the uncertainties are smaller than the size of the symbols used.

In Fig. 4, the experimental Ar-induced pressure shift coefficients (cm<sup>-1</sup>/atm at ~294 K) as a function of *m* are plotted for transitions in the 30012 $\leftarrow$ 00001 and 30013 $\leftarrow$ 00001 and the 31112 $\leftarrow$ 01101 and 31113 $\leftarrow$ 01101 bands. The pressure-shift coefficients for the 30012 $\leftarrow$ 00001 and 30013 $\leftarrow$ 00001 bands are plotted in panel Fig. 4*a*, and those for the 31112 $\leftarrow$ 01101 and 31113 $\leftarrow$ 01101 bands in panel Fig. 4*b*. The transitions belonging to the 31112 $\leftarrow$ 01101 and 31113 $\leftarrow$ 01101 bands are weak, and the measured shift coef-

**Fig. 5.** Comparison of measured Ar pressure-shift coefficients. (*a*) The measured Ar-shift coefficients for the  $30012 \leftarrow 00001$  band from present work are plotted as a function of *m* and compared with measurements for self- and air-shift coefficients from ref. 4. The experimental Ar-shift coefficients are fitted to the same empirical expression used in [2, 3] and the calculated Ar-shift coefficients are plotted by a solid curve. (*b*) The percentage differences between Ar-shift coefficients and the fitted curve are plotted as a function of *m*. (*c*) The differences (self-Ar) pressure-shift coefficients are plotted as a function of *m*. (*d*) the ratio of self- to Ar-shift coefficients are plotted as a function of *m*. The corresponding results obtained for Ar pressure-shift coefficients for the  $30013 \leftarrow 00001$  band are displayed in (*e*)-(*h*).



ficients therefore have larger uncertainties. In Fig. 4*a*, it is apparent that the shift coefficients in the bands from the ground state are significantly different in the P and R branches. For comparison, the Ar-induced shift coefficients in the  $3v_3$  band by Thibault et al. [13] are compared with present measurements in Fig. 4*a*. Those pressure-shift coefficients are more negative than present values. The Ar pressure-shift coefficients for the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands are all negative and range between  $\sim -0.002$  and -0.011 cm<sup>-1</sup>/atm at  $\sim 294$  K. The Ar pressure-shift coefficients coefficients are more negative to a structure of the compared between  $\sim -0.002$  and -0.011 cm<sup>-1</sup>/atm at  $\sim 294$  K. The Ar pressure-shift coefficients coefficients coefficients are structure and range between  $\sim -0.002$  and -0.011 cm<sup>-1</sup>/atm at  $\sim 294$  K. The Ar pressure-shift coefficients coefficients coefficients are structure and range between  $\sim -0.002$  and -0.011 cm<sup>-1</sup>/atm at  $\sim 294$  K.

efficients for the  $31112 \leftarrow 01101$  and  $31113 \leftarrow 01101$  bands are found to be slightly more positive near low *J*, although this may be due in part to the larger uncertainty in these measurements as noted above. The large scatter observed in both the Ar-broadened half-width (Fig. 2*b*), and especially the pressure-shift coefficients (Fig. 4*b*) for the hot bands, is because of the weak absorption of these lines.

In Figs. 5*a* and 5*e*, the measured  $\delta^0(Ar)$  coefficients for the 30012 $\leftarrow$ 00001 and 30013 $\leftarrow$ 00001 bands are re-plotted as a function of *m* with the self- and air- shift coefficients

**Fig. 6.** Comparison of measured Ar-broadened off-diagonal relaxation matrix element coefficients and speed dependence in  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands. (*a*) Measured off-diagonal relaxation matrix elements (cm<sup>-1</sup>/atm at 296 K) for Ar-broadening compared with previous measurements determined for self- and air-broadened off-diagonal relaxation matrix element coefficients [4, 5] plotted as a function of *m* for the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands of  ${}^{16}O^{12}C^{16}O$ . (*b*) The measured speed dependence parameters in the P- and R-branch transitions of the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands of  ${}^{16}O^{12}C^{16}O$  are plotted vs. *m*. The speed dependence parameters determined from previous analyses [4, 5] of self- and air-broadening are also displayed for comparison purpose. The speed dependence parameter is assumed to be independent of broadening gas, and a single value is used to fit each transition (see text for details). Where error bars are

not visible the uncertainties are smaller than the plot symbol.



obtained previously [4, 5] for the same transitions. The measured Ar-shift coefficients are fitted to the same form of empirical function used by Toth et al. [2, 3], and the calculated values (for Ar shift coefficients) are shown by the solid curves passing through the measured points. The percentage differences  $\delta^0(Ar)$  (obs.-calcd.), between the measured and empirically calculated pressure shift coefficients are plotted as a function of *m* in Figs. 5*b* and 5*f*. The measured and modeled values agree within ±5% with a few exceptions at low and high *J* values. The systematic nature of the point-to-point residuals, though, points to the fact that the modeled function does not fully match the measured shifts. Thus, the measured shifts should be used in preference to the modeled ones and the coefficients found for the fitted curve are not given. Figures 5*c* and 5*g* display the differences between

self- and Ar-induced shift coefficients as a function of *m*. From Figs. 5*a* and 5*e*, it is apparent that the self- and Ar-induced shift coefficients follow fairly closely to each other in the R branch and there is a nearly constant shift between the self- and Ar-induced shift coefficients in the P branch; the Ar-induced shifts being slightly more negative than the self-induced shifts. Therefore, the self shift minus Ar shift in the R branch is close to zero all the way from R0 to R56, while in the P-branch side, there is ~ +0.001 to +0.002 cm<sup>-1</sup> difference in  $\delta^0$ (self-Ar) from P2 to P56. It was not possible to find similar smooth variations in the shift coefficients as a function of *m* between air- and Ar-broadening. The dashed line corresponds to zero difference.

Figures 5d and 5h display the ratios  $\delta^0$ (self and Ar) as a function of m. The results are almost a mirror image of

those seen in the differences in the shifts in Figs. 5*c* and 5*g*. For example, in the 30012 $\leftarrow$ 00001 band, the ratio obtained in the R branch is between  $\sim 0.95$  and 1, while in the P branch the ratio varies from  $\sim 0.7$  to 1.0 from P2 to P56. The horizontal dashed lines in Figs. 5*d* and 5*h* correspond to a ratio of 1.0.

### 4.2. Ar line mixing and speed-dependent line shapes

We observed small, but persistent, systematic residuals in the multispectrum fits of Ar-broadened spectra similar to those attributed to line mixing and speed-dependent line shapes in our previous studies on self- and air-broadening [4, 5]. As done in refs. 4 and 5, we invoked line mixing by including nearest neighbor off-diagonal relaxation matrix elements in the multispectrum fit by the formulation of [33, 34], which define  $W_{ij}$ . This reduced the fitted residuals from a global standard deviation of 0.099% to 0.079%. However, some small systematic residuals remained under the line centers of the stronger transitions (P40-R40) of the  $30012 \leftarrow$ 00001 and 30013←00001 bands. These remaining residuals were removed by including speed dependence by the formulation of [34]. This further reduced the overall standard deviation of the fit from 0.079% to 0.076%. The fit residuals due to line mixing and speed dependence are different in appearance and hence distinguishable in our multispectrum fits. The effect upon the half-width coefficients by including these effects in the spectral line profile is to increase them by 2%-3%. The effect upon the pressure shift coefficients is to make them more negative by up to a few percent on the low wavenumber side of a P or R branch and up to a few percent less negative on the high wavenumber side. Near the center of the branch, the effect upon the shift coefficients is much smaller.

As an example, the final multispectrum fit interval for the  $30012 \leftarrow 00001$  band is shown in Fig. 1. Similar to [4, 5], line mixing was considered only between the nearest neighboring lines in the P and R branches; all other off-diagonal relaxation matrix elements were fixed to zero. The measured off-diagonal relaxation matrix element coefficients (cm-1/ atm at 296 K) for the  $30012 \leftarrow 00001$  and the  $30013 \leftarrow 00001$ bands are listed in Table 6. The parameters determined for self-mixing and air line mixing [4] are also given in Table 6 for comparison. It is clear that the measured off-diagonal relaxation matrix element coefficients depend upon the broadening gas; vary significantly with m and are somewhat different in the P and R branches. The off-diagonal relaxation matrix element coefficients are the largest for selfbroadening and smallest for Ar-broadening with air-broadening having intermediate values, similar to the trend observed for pressure-broadened half-width coefficients. The temperature dependences of the off-diagonal relaxation matrix elements for Ar-broadening were fixed to 0.75 to be consistent with the assumed temperature dependence exponents of pressure-broadened half-width coefficients. This introduced negligible errors in the measured line mixing parameters, since the present data were all obtained near room temperature ( $\sim 294$  K).

The measured off-diagonal relaxation matrix elements and speed dependence parameters for the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands are plotted as a function of *m* in Fig. 6. The off-diagonal relaxation matrix elements for self-, air-,

and Ar-broadening are plotted in panel Fig. 6a and the speed dependence parameters for self- and air-, and selfand Ar-broadening in panel Fig. 6b. Similar to self- and air-broadening [4, 5], the off-diagonal relaxation matrix elements beyond m = 40 were fixed to 0.004 cm<sup>-1</sup>/atm, and the speed-dependent parameters were fixed to 0.1 in the present analysis. We used a single speed dependence parameter for each transition in the multispectrum fit, since the speed dependence parameter is related to the temperature dependence of the half-width, and the same temperature dependence for both Ar- and self-broadening was assumed.

# 5. Conclusion

Experimental measurements of Ar-broadened half-width and Ar-induced pressure-shift coefficients at room temperature are reported for transitions in the  $30012 \leftarrow 00001$  and  $30013 \leftarrow 00001$  bands and for the associated hot bands transitions in  $31112 \leftarrow 01101$  and  $31113 \leftarrow 01101$ . Systematic errors in the multispectrum nonlinear least-squares analysis used in the present study are minimized by using a Voigt line shape, modified to include both line mixing and speed dependence. The measured half-width and pressure-shift coefficients from the present study are compared with similar parameters recently obtained for self- and air-broadening [4, 5].

In the present work, the same set of self-broadened spectra included in recent previous studies [4, 5] are used. Airbroadened CO<sub>2</sub> spectra used in the previous analysis were substituted with Ar-broadened CO<sub>2</sub> data. The goal in this study was to keep the same level of accuracy in the various spectroscopic line parameters as in the previous study (selfbroadening, self-induced pressure shift coefficients, self-line mixing; as well as line center positions and line intensities) and measure Ar-broadened half-width and Ar pressure-shift coefficients with the maximum possible accuracy. These new measurements of Ar-broadened half-width and Ar pressure-shift coefficients as well as line mixing due to Arbroadening should provide the best possible values available so far for remote sensing of planetary atmospheres. Accurate low-temperature pressure-broadened half-width and shift coefficients will be of great importance to atmospheric studies.

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